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Title: Phase selection during calcium silicide formation for layered and powder growth

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Abstract: Phase selection during Ca silicide formation was discussed using the chemical potential and the effective heat of formation ($\Delta H'$) models. The compositional analyses of Ca silicides were experimentally carried out in detail for both the layered and powder growth process. Based on the calculation, the Ca_2Si phase has the largest negative $\Delta H'$ and is the first phase to form in the Ca-Si system. In addition, the total energy consideration consisting of the formation energy of each phase and interfacial energy between two adjoining phases is proposed to explain the experimental results of phase selection in the Ca silicide formation.

January 18, 2011

Dear Hongge Pan, PhD, Editor,
Journal of Alloys and Compounds

I am sending herewith a revised manuscript entitled "Phase selection during calcium silicide formation for layered and powder growth" by Cuilian Wen, Akihiko Kato, Tomomi Nonomura, Hirokazu Tatsuoka, which I should like to submit for publication in Journal of Alloys and Compounds, Ms. Ref. No.: Ms. Ref. No.: JALCOM-D-10-06110R1.

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November 13, 2010

Prime Novelty Statement,

We confirm that:

1. This manuscript is the authors' original work and has not been published nor has it been submitted simultaneously elsewhere,
2. That all authors have checked the manuscript and have agreed to the submission.

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Title: Phase selection during calcium silicide formation for layered and powder growth
Journal of Alloys and Compounds

Dear Hongge Pan, PhD, Editor
Journal of Alloys and Compounds

Thank you very much for your editing the manuscript. The manuscript was sincerely revised according to the editor's comments. The editor's comments and Author's replies are as follows.

Editor's comment 1,

1 The title should be corrected into "Phase selection during calcium silicide formation for layered and powder growth". In the title and subtitles, the first word should begin with a capital letter and the others should be in lower-case letters.

Author's reply 1,

The title is corrected into "Phase selection during calcium silicide formation for layered and powder growth". Thank you for this notice.

Editor's comment 2,

In the section of the References, the "J. Alloys Comp." should be modified into "J. Alloys Compd."

Author's reply 2,

In the section of the References, the "J. Alloys Comp." is modified into "J. Alloys Compd."

Editor's comment 3,

Numerous relevant papers have been published in the Journal of Alloys and Compounds (J. Alloys Compd.) and other Journals since 2009 especially since 2010. Some key, important or/and latest research results should be mentioned and cited in the section of introduction instead of outdated or earlier papers so that we can provide a solid background and progress to the readers regarding the current state-of-knowledge on this topic. Therefore, I strongly require you to rewrite this part and then update your citations, or it is very hard for me to accept your manuscript.

Author's reply 3,

Thank you very much for this suggestion. The important and latest research results should be mentioned as pointed out by the editor. I additionally mention the following descriptions in 1. Introduction, and new papers are added in References.

“The phase formation and transformation of multi-component compound systems have been intensively discussed based on thermodynamic considerations [1-8]. For the case of phase formation and phase stability, thermodynamic descriptions were

developed using thermodynamic models for Cr-Sn-Ti [1] and Al-Zn-Mg-Si [2]. The chemical potentials consideration was made for the growth of gold-seeded III-V semiconductor nanowires [3]. On the other hand, for the case of growth phase evolution, the preferable phase formation or phase selection was investigated under the consideration of thermodynamics for Mg-Sn-Si and Mg-Sn-Si-Ca [4] and Fe-Co [5]. The phase transformation or the solidification pathways was investigated for from anatase to rutile [6], Mg-Pd nanoparticles [7] and Mg-Zn-Y-Zr alloys [8].”

- [1] Y.L. Gao, C.P. Guo, C.R. Li, Z.M. Du, J. Alloys Compd. **498** (2010) 130.
- [2] Q. Li, Y.Z. Zhao, Q. Luo, S.L. Chen, J.Y. Zhang, K.C. Chou, J. Alloys Compd. 501 (2010) 282.
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- [8] Z.H. Huang, S.M. Liang, R.S. Chen, E.H. Han, J. Alloys Compd. **468** (2009) 170.

Ref. 4 is now in press, but it can be seen in ScienceDirect Website;
doi:10.1016/j.jallcom.2010.12.052

Editor's comment 4,

Any changes or revisions in the text should be highlighted by different color in the revised manuscript compared with that of the previous version.

Author's reply 4,

Changes and revisions in the text shown in red color in the revised manuscript.

Phase selection during calcium silicide formation for layered and powder growth

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Abstract

Phase selection during Ca silicide formation was discussed using the chemical potential and the effective heat of formation ($\Delta H'$) models. The compositional analyses of Ca silicides were experimentally carried out in detail for both the layered and powder growth process. Based on the calculation, the Ca_2Si phase has the largest negative $\Delta H'$ and is the first phase to form in the Ca-Si system. In addition, the total energy consideration consisting of the formation energy of each phase and interfacial energy between two adjoining phases is proposed to explain the experimental results of phase selection in the Ca silicide formation.

Keywords: Interfaces; Growth from vapor; Calcium compounds;

Semiconducting silicon compounds

1. Introduction

Recently, semiconducting silicides have attracted much attention as environmentally conscious materials, which consist of non-toxic and abundant materials. The solid phase interaction between thin metal films and silicon has been widely studied because of the importance of silicides as interconnects and contacts in silicon devices.

The phase formation and transformation of multi-component compound systems have been intensively discussed based on thermodynamic considerations [1-8]. For the case of phase formation and phase stability, thermodynamic descriptions were developed using thermodynamic models for Cr-Sn-Ti [1] and Al-Zn-Mg-Si [2]. The chemical potentials consideration was made for the growth of gold-seeded III-V semiconductor nanowires [3]. On the other hand, for the case of growth phase evolution, the preferable phase formation or phase selection was investigated under the consideration of thermodynamics for Mg-Sn-Si and Mg-Sn-Si-Ca [4] and Fe-Co [5]. The phase transformation or the solidification pathways was investigated for from anatase to rutile [6], Mg-Pd nanoparticles [7] and Mg-Zn-Y-Zr alloys [8].

For considering the silicide growth, there has been considerable interest in formulating rules for predicting the first silicide phase which forms as well as the sequence of subsequent phases [9-11]. These rules heavily rely on phase diagram information such as the lowest eutectic, stability and diffusion species, but do not directly use thermodynamic data. Some metal-silicons, such as the Cr-Si, Co-Si and Ni-Si systems have been extensively discussed [11-13]. However, there are few reports on the phase selection during the silicide formation of the Ca-Si system. Ca silicide powders and films have been grown on Si or Si/Mg₂Si powders or substrates by heat diffusion treatments [14-18], however, it is still difficult to grow high quality single phase Ca silicide. There are multiple silicide phases, such as CaSi₂, CaSi, Ca₅Si₃ and Ca₂Si that exist in the Ca-Si system, which could lead to the simultaneous formation during its growth [14-17]. Among them, Ca₂Si and Ca₅Si₃ have been reported to have a semiconducting behavior [14, 15, 19]. It is important to understand the elemental chemical potential gradients and effective heat of formation (EHF) as certain driving forces for diffusion in the Ca-Si system, in addition to the concentration controlled phase selection.

Experimentally, Ca-silicide formations were reported in refs. 16 and 19, which reported for the

layered growth, the Ca_2Si and CaSi interface was formed while the Ca_5Si_3 phase was not significantly formed. On the other hand, for powder growth, the Ca_5Si_3 single phase powders were grown. However, a detailed compositional analysis has not been carried out.

In this study, the compositional analysis of Ca-silicides was made for both the layered and powder growth processes. In addition, the phase selection during the Ca silicide formation was discussed based on the chemical potential and the effective heat of formation ($\Delta H'$) models associated with the additional interfacial energy to explain the experimental Ca silicide layered and powder growth processes.

2. Experimental

As the first step in the silicide layer growth, Mg_2Si layers were grown on Si substrates prior to the Ca_2Si growth. The Mg source and Si substrates were placed in a loosely sealed quartz container, which was loaded into a vacuum chamber. The container was then heated and the temperature was maintained at 370°C . The growth procedure of the Ca_2Si layer is basically the same as the Mg_2Si growth, except for the growth temperature and growth time. The Ca_2Si layers were grown by the heat treatment of $\text{Mg}_2\text{Si}/\text{Si}(1\ 1\ 1)$ substrates at 600°C in Ca vapor for 3 h [16].

The Ca_5Si_3 powders were synthesized by exposure of the Si powder to Ca fluxes. The Ca source and Si powder were first placed in a loosely sealed glass container, and then the container was loaded into a vacuum chamber. The container was then heated and the temperature was maintained at 750°C for 12 h [19].

The structural properties of the resultant layers and powders were characterized by scanning electron microscopy (SEM) measurements. In addition, the compositional analysis was completed using energy dispersive X-ray spectroscopy (EDS).

The two-dimensional chemical potential diagram of the CaSi_2 , CaSi , Ca_5Si_3 and Ca_2Si phases for the Ca-Si system was calculated by a first principles scheme based on the local density functional theory. It was postulated that the Ca_mSi_n phase is grown under thermodynamically equilibrium conditions which is characterized by the chemical potentials of the constituent elements, μ_{Ca} and μ_{Si} . The following expression should be satisfied:

$$\mu_{\text{Ca}_m\text{Si}_n} \leq m\mu_{\text{Ca}} + n\mu_{\text{Si}}, \quad (1)$$

where $\mu_{\text{Ca}_m\text{Si}_n}$ is the chemical potential of Ca_mSi_n per one chemical formula. Furthermore, if no segregation in Ca_mSi_n occurred, the following conditions should be added:

$$\begin{aligned} \mu_{\text{Ca}_m\text{Si}_n} &= m\mu_{\text{Ca}}^{\text{bulk}} + n\mu_{\text{Si}}^{\text{bulk}} - \Delta G_{\text{Ca}_m\text{Si}_n}, & \Delta G_{\text{Ca}_m\text{Si}_n} &> 0, \\ \mu_{\text{Ca}} &< \mu_{\text{Ca}}^{\text{bulk}}, & \mu_{\text{Si}} &< \mu_{\text{Si}}^{\text{bulk}}, \end{aligned} \quad (2)$$

where $\mu_{\text{Ca}}^{\text{bulk}}$ and $\mu_{\text{Si}}^{\text{bulk}}$ are the chemical potentials of bulk Ca and Si crystals, respectively, and $\Delta G_{\text{Ca}_m\text{Si}_n}$ is the heat of formation. The $\mu_{\text{Ca}_m\text{Si}_n}$, $\mu_{\text{Ca}}^{\text{bulk}}$ and $\mu_{\text{Si}}^{\text{bulk}}$ values were obtained by first principles total energy calculations (the entropy contributions was neglected). Our total energy calculation scheme is described in ref. 20.

3. Results and discussion

The two-dimensional chemical potential diagram for Ca silicide phases is shown in Fig. 1. The stable domain of each stoichiometric phase is defined by a line, because the sum of the chemical potentials of the different components weighted by the appropriate stoichiometric coefficient is equal to the Gibbs energy of formation of the phase. The points of intersection of the two lines identify the two-phase equilibriums. The planes, defined by the intersection of the corresponding lines, represent the corresponding phase's coexisting field. It is noted that the stable domain of the single-phase only existed in the line of no planes with the other lines, called the single-phase line. It was found that all of the binary phases mentioned here have a certain stable domain as shown by the single-phase lines in the figure. In addition, it is noted that the CaSi_2 , CaSi , and Ca_2Si have relatively larger stable single-phase domains compared to the Ca_5Si_3 phase, which suggests that the Ca_5Si_3 single-phase formation window is narrower than that of the other phases.

The heats of formation (ΔH^0) of the Ca silicide phase is calculated from the potential energies shown in Fig. 1 according the formula shown below:

$$\mu_{\text{Ca}_m\text{Si}_n} = m\mu_{\text{Ca}} + n\mu_{\text{Si}} - \Delta G_{\text{Ca}_m\text{Si}_n}. \quad (3)$$

Assuming the equilibrium condition, $\Delta G_{\text{Ca}_m\text{Si}_n} = 0$, $\mu_{\text{Ca}_m\text{Si}_n}$ is the chemical potential for

$m \times \mu_{\text{Ca}} + n \times \mu_{\text{Si}}$ in the Ca_mSi_n phases. From Fig. 1, it is calculated as -1.44, -1.34, -4.84 and -1.70 eV for CaSi_2 , CaSi , Ca_5Si_3 and Ca_2Si , respectively. The heat of formation energy for 1 mol is obtained as:

$$\Delta H^0 = N_A \times \mu_{\text{Ca}_m\text{Si}_n}, \quad (4)$$

where N_A is the Avogadro constant of $6.02 \times 10^{23} \text{ mol}^{-1}$. The calculated heat of formation energy for each phase is listed in Table 1. In addition, most available phase equilibriums and thermodynamic data for the Ca-Si system have been collected and critically evaluated by M. Heyrman et al [21]. Some ΔH^0 calculated from the literature [22-24] is also shown in the table, which is in excellent agreement with our calculated results.

The driving force for a process to take place is given by the change in the Gibbs free energy:

$$\Delta G = \Delta H - T\Delta S, \quad (5)$$

where ΔH is the change in enthalpy (or heat of formation) during the reaction at temperature T and ΔS is the change in entropy. For the solid state interactions, $\Delta S \approx 0$ and ΔG is thus approximated by the change in ΔH during the reaction. However, the first formed phase is not only determined by the lowest heat of formation, but also by the concentration of atoms at the growth interface available to participate in the reaction. The effective concentration differs from the physical concentration at the growth interface and cannot be directly calculated [12, 25-27]. The effective heat of formation ($\Delta H'$) of the Ca silicide phases is calculated as a function of the concentration, and is given by the Ca-Si phase diagram in Fig. 2. A general definition of the $\Delta H'$ is given in ref. 11. It is clear that all the phases have a negative $\Delta H'$ and thus the release of the energy from the system occurs when the concentrations of Ca and Si match that of the composition of a particular compound. In order to determine the phase that will be formed, it is necessary to know the effective concentration of the elements at the growth interface. Generally, the intermixing at the interface during the solid phase reaction is expected to take place at the concentration of the lowest temperature eutectic of the binary system. In the case of the Ca-Si system, this occurs at a composition of 3.5 at% Si as shown in Fig. 2.

A rule for the first phase formation can thus be formulated which state the following: the first silicide compound to form during the metal-silicon interaction is the congruent phase with the

most negative $\Delta H'$ at the concentration of the lowest temperature eutectic of the binary system [11]. The value of $\Delta H'$ has been calculated for the Ca-Si system at the lowest melting eutectic composition in Table 1. It is shown that CaSi has the largest negative ΔH° of -15.6 kcal/g atom. However, at the lowest temperature eutectic point (3.5 at% Si), the limiting element is Si, and the Ca_2Si phase has the largest negative $\Delta H'$ of -1.4 kcal/g atom. Thus, it is expected that Ca_2Si is to be the first phase to form in the Ca-Si system.

During the normal Ca silicide formation, the effective concentration at the growth interface is controlled by the lowest eutectic. At this concentration, according to the EHF model, it can be seen that Ca_2Si has the largest negative $\Delta H'$ and is expected to form first as shown in Fig. 2. For thin Ca on thick silicon, all the Ca will be consumed to form Ca_2Si , and the effective concentration moves to the right side of the EHF diagram. According to the theory, Ca_5Si_3 formation should lead to the largest negative $\Delta H'$ until the effective concentration is about 65 at% Ca is reached. After complete transformation of Ca_2Si to Ca_5Si_3 , the effective Ca concentration at the growth interface further decreases to a concentration of less than about 55 at% Ca, thus the CaSi formation is thermodynamically favored. While after reaching 35 at% Ca, CaSi_2 formation is favored.

To examine the phase selection during the Ca silicide formation for the layered growth experimentally, selection of the substrate material is important to obtain the Ca-silicide layered structure. For the growth of Ca-silicide layers directly on Si substrates, the resultant Ca-silicides were easily removed from the Si substrates by an external stress, because of the formation of CaSi_2 phase with trigonal-rhombohedral stacking sequence structure, as reported previously [16]. On the other hand, Ca_2Si layers were successfully grown on $\text{Mg}_2\text{Si}/\text{Si}$ substrates [16]. Thus, the $\text{Mg}_2\text{Si}/\text{Si}$ substrates were employed for the Ca-silicide layered growth.

Figure 3 shows the cross-sectional SEM micrograph and the corresponding EDS analysis for the $\text{Ca}_2\text{Si}/\text{CaSi}$ interface made by the Ca-silicide layered growth. It is found that no evidence of the formation of the Ca_5Si_3 phase is observed between the Ca_2Si and CaSi layers.

As shown in Figs. 1 and 2, Ca_5Si_3 is one of stable phases, though the Ca_5Si_3 single-phase formation window is narrower than that of the other phases. However, the un-formation of the Ca_5Si_3 phase cannot be explained by the formation energy of each material.

In fact, it is possible to grow the Ca_5Si_3 phase as shown in Fig. 4, which shows the SEM micrograph and the corresponding EDS analysis for the particles of the resulting powders. The powders are confirmed to be Ca_5Si_3 by the XRD spectrum in ref. 19. The morphology and the EDS analysis showed powder size of about $\sim 200\text{ }\mu\text{m}$ and the compositionally homogeneous compound is formed through the powders.

Even though the Ca_5Si_3 phase has a narrower growth window as shown in Figs. 1 and 2, if the appropriate Ca and Si concentration ratio and the growth condition could be preferably chosen, the Ca_5Si_3 single-phase compound can be successfully obtained, as expected for the second nucleation phase in the EHF consideration. For the powder growth, when the powder size is smaller, the boundary condition is not fixed, and the composition of any part of the powder can be maintained at the same composition, and the composition of the powder is determined by the growth conditions.

On the other hand, not only Ca_2Si , but also the CaSi phase was grown, and formation of the Ca_5Si_3 phase was skipped during the experiment. The EHF consideration does not explain this phenomenon, but might be explained as follows. For the layered growth, the boundary conditions are always fixed, for example, the Ca-silicide phases are formed between the Si substrate and the deposited Ca. This growth condition causes the formation of a layered structure with a distinct compositional gradient from the substrate to the layer surface. The domains or substrates with 100% Si always exist on one side of the reaction region. It is considered that the Si rich silicide phases are formed when the Ca flux through the silicide layers to Si layers (substrate) decreases. It would also be possible that the second lowest eutectic affects the silicide formation in the Si-rich region.

As already mentioned, the formation energy consideration cannot explain the formation of the $\text{Ca}_2\text{Si}/\text{CaSi}$ structure. The total energy consideration consisting of the formation energy of each phase and interfacial energy between two adjoining phases is proposed to explain the formation of the structure. As shown in Fig. 3, the $\text{Ca}_2\text{Si}/\text{CaSi}$ interface is formed, while no formation of the Ca_5Si_3 phase is observed for the layered growth. The structure is schematically illustrated in Fig. 5(a).

Assuming that a part of the $\text{Ca}_2\text{Si}/\text{CaSi}$ interface region is transformed into the Ca_5Si_3 phase, a

Ca₅Si₃ layer with a thickness of $c=1.46$ nm (the largest lattice constant) between the Ca₂Si and CaSi regions is formed, as shown in Fig. 5(b). The phase transformation reaction is shown as:

The number of Ca and Si atoms should be equal for both cases shown in Figs. 5(a) and (b). Thus, the amounts of the substances in each region should be $n_{A2} \text{ (mol)} = 2 \times n_{B1} \text{ (mol)}$ and $n_{C2} \text{ (mol)} = n_{B1} \text{ (mol)}$. Assuming the interface area of the layers is a unit area, namely, 1cm^2 , the calculated amounts of the substances are shown in the Fig. 5 table. The A1 and C1 layers are not listed, because the internal energy is not changed for the cases whether or not Ca₅Si₃ is formed.

The sum of the internal energy deduced from the heat of formation energy in each region, A₂, C₂ and B₁, are -8.95×10^{-8} , -3.55×10^{-8} and -1.28×10^{-7} kcal, respectively. Comparing the internal energy for (a) $E_{A2+C2} = -1.25 \times 10^{-7}$ kcal with that for (b) $E_{B1} = -1.28 \times 10^{-7}$ kcal, the case (b) Ca₂Si/Ca₅Si₃/CaSi structure is more thermodynamically favored than the case (a) Ca₂Si/CaSi structure, which is not consistent with the previously reported experimental results.

However, it should be pointed out that another new interface is formed when Ca₅Si₃ exists, namely, there is one interface for (a) Ca₂Si/CaSi, and there are two interfaces for the (b) Ca₂Si/Ca₅Si₃/CaSi structures. Actually, it is difficult to calculate the interface energy for the Ca silicides. However, it is worthwhile to refer the typical values of interfacial energy for the reported silicide materials. It has been reported that the TiSi₂ interfaces energies are 900 ergs/cm² on silicon (100) and 600 ergs/cm² on silicon (111), respectively. For ZrSi₂, the interfaces energy is 800 ergs/cm² on silicon (111) [29]. Assuming that the interface energy E_{surf} is typically 800 ergs/cm², namely 1.91×10^{-8} kcal/cm², the total energy including the sum of the heat of formation energy and the interfacial energy are for (a) $E_{A2+C2} + E_{\text{surf}} = -1.06 \times 10^{-7}$ kcal and for (b) $E_{B1} + 2 \times E_{\text{surf}} = -8.93 \times 10^{-8}$ kcal. The result suggests that the formation of the interface increases the total energy of the structure. In this calculation, the actual values of the Ca silicide interfaces are not clear, however, it is certain that the additional interface formation increases the total energy of the structure, thus a multilayer structure does not tend to be realized. Thus, it could be concluded that the Ca₅Si₃ would not form between the Ca₂Si and CaSi layers when considering the narrower growth window of the Ca₅Si₃ as shown in Fig. 1.

4. Conclusions

Phase selection during calcium silicide formation was discussed using the chemical potential and the effective heat of formation ($\Delta H'$) models. The phase selection theory and Ca silicide interface model are discussed and compared to the experimental results. Experimentally, for the layered structure, no Ca_5Si_3 phase was formed between the Ca_2Si and CaSi phases. On the other hand, the single Ca_5Si_3 phase was formed during powder growth, and the stoichiometry distribution of the Ca_5Si_3 is homogeneous throughout the powders. In the calculation, the Ca_2Si phase has the largest negative $\Delta H'$ with the value of -1.4 kcal/g atom at the lowest temperature eutectic point (3.5 at% Si) and the first phase to form in the Ca-Si system. The proposed phase selection model including the potential energy and the additional interfacial energy successfully explains the experimental results, in which the Ca_5Si_3 phase would not form between the Ca_2Si and CaSi layers.

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Figure Captions

Fig. 1 The calculated two-dimensional chemical potential diagram of CaSi_2 , CaSi , Ca_5Si_3 and Ca_2Si phases for the Ca-Si system. The origins of each chemical potential are set to the bulk ones, $\mu_{\text{Ca}}^{\text{bulk}}$ and $\mu_{\text{Si}}^{\text{bulk}}$.

Fig. 2 The effective heat of formation ($\Delta H'$) and phase diagram [28] for the Ca-Si system. Each triangle in the effective heat of formation diagram represents the energy released as a function of the concentration during the formation of a particular calcium silicide phase.

Fig. 3 The cross-sectional SEM micrograph and the corresponding EDS analysis for the resulting layers grown at 600°C for 3h.

Fig. 4 SEM micrograph and the corresponding EDS analysis for the particles of the resulting powders grown at 750°C for 12h.

Fig. 5 Silicide formation model of $\text{Ca}_2\text{Si}/\text{Ca}_5\text{Si}_3/\text{CaSi}$ and $\text{Ca}_2\text{Si}/\text{CaSi}$ layer structures, and the corresponding calculated internal energy of the each phase.

Table 1 Heats of formation (ΔH°) and the effective heat of formation ($\Delta H'$) calculated for the lowest-melting eutectic composition for the Ca-Si system.

Phase selection of Ca silicide formation was discussed using the chemical potential.

Composition of Ca silicides was experimentally examined.

Total energy consideration is proposed to explain the experimental results.

Table 1:

Phase	Composition	ΔH°		Limiting $\Delta H'$ element (kcal/g at.)	ΔH° [14] (kcal/g at.)	ΔH° [15] (kcal/g at.)	ΔH° [16] (kcal/g at.)	
		(kcal/g mol)	(kcal/g at.)					
Lowest eutectic = $\text{Ca}_{0.965}\text{Si}_{0.035}$								
CaSi_2	$\text{Ca}_{0.333}\text{Si}_{0.667}$	-33.4	-11.1	Si	-0.6	-12.0	-9.0	-12.0
CaSi	$\text{Ca}_{0.500}\text{Si}_{0.500}$	-31.1	-15.6	Si	-1.1	-18.0	-11.9	-14.4
Ca_5Si_3	$\text{Ca}_{0.625}\text{Si}_{0.375}$	-111.8	-14.0	Si	-1.3	—	-13.2	—
Ca_2Si	$\text{Ca}_{0.667}\text{Si}_{0.333}$	-39.2	-13.1	Si	-1.4	-16.7	-13.4	-16.7

Figure 1
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Figure 2
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Figure 3
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Position	Phase	Length (nm)	n (mol)	Energy (kcal)
B1	Ca ₅ Si ₃	1.46	1.14×10 ⁻⁹	-1.28×10 ⁻⁷
A2	Ca ₂ Si	1.14	2.28×10 ⁻⁹	-8.95×10 ⁻⁸
C2	CaSi	0.33	1.14×10 ⁻⁹	-3.55×10 ⁻⁸