Performance Intensification of CO2 Methanation by Co-Feeding Oxygen Over Various Ru-Based Catalysts

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# RESEARCH ARTICLE

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# Performance Intensification of CO<sub>2</sub> Methanation by Co-Feeding Oxygen Over Various Ru-Based Catalysts

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#### ABSTRACT

Auto-methanation (AM), which autonomously progresses at room temperature (approximately 25 °C), is an effective reaction for converting  $CO_2$  to  $CH_4$  and can thus reduce the processing costs. In this study, the AM reaction over various Ru-based catalysts with different support materials positively proceeded by selecting reaction conditions such as the O<sub>2</sub> concentration and gas flow rate. The progression of AM was the best over the Ru/CeO<sub>2</sub> catalyst, followed by the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts. The progression of AM over the Ru/SiO<sub>2</sub> catalyst was slow. The rapid progress of AM over the Ru/CeO<sub>2</sub> catalyst was attributed to the presence of oxygen defects on the CeO<sub>2</sub> support that accelerates the hydrogen-oxygen combustion as well as to the differences in the CO<sub>2</sub> and H<sub>2</sub>O adsorption characteristics between the CeO<sub>2</sub> support and other supports. Even when the Ru-based catalyst underwent H<sub>2</sub> reduction at low temperature, AM could proceed over each catalyst. The Ru/CeO<sub>2</sub> catalyst was advantageous over other catalysts because AM proceeds only when H<sub>2</sub> gas is supplied at room temperature without external heating. X-ray photoelectron spectroscopy indicated that the Ru species on the Ru/CeO<sub>2</sub> catalyst are in a metallic state owing to H<sub>2</sub> reduction at room temperature, which is associated with AM progression. Moreover, AM proceeded via  $H_2$  reduction at 75 °C over the Ru/ZrO<sub>2</sub> catalyst and at 150 °C over the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst. The progression of methanation through such low-temperature reduction can strengthen the CO<sub>2</sub> conversion process.

# 1. Introduction

The development of process technologies related to the reduction and utilization of greenhouse gases is an important research field from the perspective of global environmental conservation. Research on carbon capture and storage (CCS) and carbon capture and utilization (CCU) for the purpose of CO<sub>2</sub> reduction has been actively conducted, and large-scale projects have been promoted in recent years. Jupiter 1000 (https://www.jupiter1000.eu/), STORE & GO (https://www.storeandgo.info/), and ALIGN CCUS (https:// www.alignccus.eu/) in Europe are examples of such projects. As CO<sub>2</sub> reduction and utilization techniques, methanol synthesis and dimethyl ether synthesis from CO<sub>2</sub> and H<sub>2</sub> are taken up in the ALIGN CCUS project, and CO<sub>2</sub> methanation is taken up in the Jupiter 1000 and STORE & GO projects.

 $CO_2$  methanation ( $CO_2 + 4H_2 \rightarrow CH_4 + 2H_2O$ ,  $\Delta H^0_{298} = -165 \text{ kJ/mol}$ ) is a reaction that Paul Sabatier reported in the early 20th century (Sabatier and Senderens 1902). Recently, it has received attention as a reaction that reduces  $CO_2$  emitted from industrial processes and produces a

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resource such as methane. In this reaction, CO<sub>2</sub> is converted to CH<sub>4</sub> via reduction with eight electrons. For accelerating the reaction, many studies have used a Ni-based, Ru-based, or Co-based catalyst while supplying thermal energy of 250-400 °C to the reaction field. However, the reduction of the supplied thermal energy, that is, the reduction of the reaction temperature, during methanation is challenging. To solve this problem, research on the development of highperformance catalysts is being actively conducted from the viewpoint of catalyst design, which mainly involves selection of the active components and catalyst preparation methods. Concrete studies have been summarized in several review articles based on the development of methanation catalysts (Ghaib et al. 2016; Rönsch et al. 2016; Younas et al. 2016; Frontera et al. 2017; Ashok et al. 2020; Lee et al. 2021). Although there are differences in reaction conditions and catalyst bed conditions, accelerating methanation at approximately 200 °C is one of the development goals for designing low-temperature catalysts.

Additionally, for the treatment of  $CO_2$  emitted from industrial processes by methanation, the development of a catalytic reaction system that enables the handling of a large

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amount of CO<sub>2</sub> gas and the efficient control of the large amount of exothermic energy associated with the reaction is imperative. These functions are not exhibited by conventional catalyst packed-bed systems, rendering them unsuitable for industrial CO<sub>2</sub> treatment. To address the aforementioned challenges, we have developed a structured catalyst system with excellent heat transfer and a lower pressure loss during the reaction (Fukuhara and Igarashi 2004, 2005; Fukuhara et al. 2005, 2007; Fukuhara and Ohkura 2008; Fukuhara and Kawamorita 2009; Fukuhara et al. 2013, 2015). This is a honeycomb- or spiral-type structured catalyst system onto which an Ni- or Cu-based catalyst component is attached. We reported that this catalytic system allows efficient control of thermal energy and processing of large amounts of CO<sub>2</sub> and is advantageous for deployment in industrial processes (Fukuhara et al. 2017; Ratchahat et al. 2018; Fukuhara et al. 2019). Structured catalysts include the foam-type, plate-type, and sponge-type catalysts; the methanation characteristics of these catalysts were reviewed by Huynh and Yu (2020). From the viewpoint of efficient control of the exothermic energy of methanation, the utilization of a microreactor system is an effective method. Because this reactor system is compact, the exothermic energy and mass transfer of the raw-material gas can be controlled relatively easily. It is expected to facilitate intensification of the methanation process.

For accelerating methanation, heat energy is generally supplied to the reaction field by applying a heating device such as an electric furnace from the outside. The external heating method is also widely used for other catalytic reactions. While, we succeeded in accelerating methanation by co-supplying oxygen gas with a raw-material gas and by using the exothermic energy of hydrogen combustion, maintaining a high methane yield (Fukuhara, Ratchahat, Kamiyama et al. 2019; Fukuhara, Ratchahat, Suzuki et al. 2019; Fukuhara et al. 2020; Hirata et al. 2020). Additionally, we discovered that this heating method autonomously activates methanation at room temperature (approximately 25 °C) and have termed this phenomenon as auto-methanation (AM). The exhaust gas from industrial processes contains not only CO<sub>2</sub> but also large amounts of O<sub>2</sub>, N<sub>2</sub>, CO, and other gases; thus, an additional process for separating and concentrating CO<sub>2</sub> is generally proposed. The maintenance and operation of this separation/enrichment equipment increase the process cost. If the emitted CO<sub>2</sub> gas can be treated by methanation while O2 and CO are mixed, the separation and concentration processes become unnecessary, simplifying the process equipment and reducing the construction cost. Furthermore, AM leads to process intensification of CO<sub>2</sub> treatment systems, because autonomous activation and operation of methanation in the room-temperature region significantly reduce the running costs. To understand the possible reasons why CH<sub>4</sub> produced via methanation does not burn in the co-supplied O<sub>2</sub> gas, the order of the minimum ignition energy for the hydrogenoxygen mixed gas and the methane-oxygen mixed gas was considered (Lewis and Elbe 1961). It was found that because the combustion rate of the hydrogen-oxygen mixed gas is rapid, the combustion of the produced methane does not proceed. We experimentally confirmed the flame retardancy of methane in the presence of  $O_2$  in a previous study (Hirata et al. 2020). We have confirmed the occurrence of such an AM phenomenon using Ni-based catalyst and Rubased catalyst. When the reaction temperature was changed from the higher side to the lower side, AM occurred even at approximately 25 °C (without external heating) over Ni- and Ru-based catalysts with CeO<sub>2</sub>, ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, and MgO as supports (Fukuhara et al. 2020). Moreover, when the reaction field was maintained at approximately 25 °C from the beginning, AM was confirmed to occur over the Ru/CeO<sub>2</sub> catalyst (Hirata et al. 2020). However, the applicability of other catalysts for AM has not yet been verified.

Therefore, in this study, we investigated the activation characteristics of methanation on the low-temperature range (25-100 °C) by using several Ru-based catalysts with different support materials. Additionally, the relationship between the physicochemical properties of the catalyst and the occurrence of AM was investigated, with a focus on hydrogen combustion. The results indicated that the Ru/CeO<sub>2</sub> catalyst showed the highest activity toward AM, followed by the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts, whereas Ru/SiO<sub>2</sub> catalyst showed the lowest activity. One of the reasons why Ru/CeO<sub>2</sub> catalyst is active toward AM is the deficiency of lattice oxygen in the CeO<sub>2</sub> support. Additionally, it was considered that the Ru/CeO<sub>2</sub> catalyst was easily reduced in the room-temperature region (without external heating) to form metallic Ru, which was also responsible for the easy starting of AM.

#### 2. Experimental

#### 2.1 Preparation of ruthenium-based catalyst

The catalysts used in this study were Ru/CeO<sub>2</sub>, Ru/ZrO<sub>2</sub>, Ru/Al<sub>2</sub>O<sub>3</sub>, and Ru/SiO<sub>2</sub>, which were prepared via the evaporation-to-dryness method. Ruthenium nitrate (Ru(NO<sub>3</sub>)<sub>3</sub>, Tanaka Kikinzoku Kogyo K. K., Ru: 50 g/L) was used as a Ru source. The loading amount of the Ru component was 10 wt% on an oxide support material. The oxide materials were CeO<sub>2</sub> (labeled JRC-CEO-2), ZrO<sub>2</sub> (labeled JRC-ZRO-3), Al<sub>2</sub>O<sub>3</sub> (labeled JRC-ALO-8), and SiO<sub>2</sub> (labeled JRC-SIO-4), which were provided by the Catalysis Society of Japan. The evaporation-to-dryness method involved the sequential combination of the stirring reagent in distilled water, the evaporation of the solvent at approximately 80 °C, and the calcination of the power product. The preparation method was described in our previous report (Fukuhara et al. 2020; Hirata et al. 2020).

# 2.2 Performance test of methanation

The  $CO_2$  methanation performance of the prepared Ruloaded catalysts was investigated using a conventional flowtype reactor under the atmospheric pressure. The reactor comprised a quartz tube with an inner diameter of 8 mm. The amount of the Ru-loaded catalyst packed into the

reactor ranged from 300 to 750 mg. A three-independentzone electric furnace (Asahi Rika Co., ARF) was used for supplying heat energy to the reactive zone. The Ru-loaded catalyst was reduced in the reactor with a H<sub>2</sub> stream of 100 mL/min for 1 h. The reduction temperature was changed from room temperature to 500 °C. Herein, "room temperature" implies no external heating. After the reduction of the catalyst, the CO<sub>2</sub> methanation performance was investigated by feeding a raw-material gas into the reactor at room temperature or 50-75 °C. The raw-material gas was composed of CO<sub>2</sub>, H<sub>2</sub>, O<sub>2</sub>, and N<sub>2</sub> (balance). The CO<sub>2</sub> concentration was fixed at 10 vol%, the O2 concentration was varied from 0 to 10 vol%, and the H<sub>2</sub> concentration was varied from 40 to 60 vol%. The total flow rate of the rawmaterial gas was varied from 200 to 800 mL/min. The gas hourly space velocity (GHSV) was varied from 24,000 to  $96,000 \,\mathrm{h^{-1}}$ . The conditions of each experiment are shown in the figure sections. To confirm the reproducibility, all performance tests were conducted two or more times under every reaction condition. The outlet gas was analyzed through gas chromatography (GC-8AIT, TCD, Shimadzu). The detected gases were CH<sub>4</sub>, H<sub>2</sub>O, CO<sub>2</sub>, and CO under all reaction conditions. The fed oxygen was completely consumed during the reaction. No other products were detected. In all reaction runs, the carbon-based material balance was almost 100%. Therefore, the CO<sub>2</sub> conversion and product selectivity were calculated according to the carbon content, by using the following equations:

$$CO_{2} \text{ conversion } (\%)$$

$$= \left(1 - \frac{\text{Molar exhaust rate of } CO_{2} \text{ at the outlet}}{\text{Molar feeding rate of } CO_{2} \text{ at the inlet}}\right) \times 100$$
(2)

 $CH_4 \text{ selectivity } (\%)$   $= \frac{\text{Molar production rate of } CH_4 \text{ at the outlet}}{\text{Molar rate of carbon} - \text{containing material at the outlet}} \times 100$ 

CO selectivity (%)

$$=\frac{\text{Molar production rate of CO at the outlet}}{\text{Molar rate of carbon - containing material at the outlet}} \times 100$$
(4)

(3)

## 2.3 Physicochemical measurement

The electronic states of the elements on the catalyst surface were measured via X-ray photoelectron spectroscopy (XPS; Axis Ultra DLD, Shimadzu, X-ray source: AlK $\alpha$  (1486.6 eV)). The XPS measurements were performed under *in situ* conditions via hydrogen reduction (temperature: 25–500 °C; holding time: 1 h) in the pretreatment part attached to the device. The specific surface area of the catalyst was measured using the Brunauer–Emmett–Teller (BET) method (3-Flex, Micromeritics) with liquid nitrogen. The amount of Ru

loaded was measured via X-ray fluorescence analysis (Supermini200, Rigaku, Inc.). The temperature desorption behaviors of CO<sub>2</sub> and H<sub>2</sub>O were determined by using a catalyst evaluation device (TPD, BELCAT II + CATCryo, Microtrac BEL) equipped with a mass spectrometer. The reduction tendency of the catalyst and the metal surface area of Ru were also determined using this device, that is, H<sub>2</sub>-TPR and CO-pulse. The crystalline states of the Ru/CeO<sub>2</sub> catalyst before and after the reaction were measured through X-ray diffraction (Ultima IV, Rigaku, Inc.) analysis with CuK $\alpha$  radiation ( $\lambda$  = 1.54 Å).

## 3. Results and Discussion

## 3.1 Startup property of methanation under O<sub>2</sub> cofeeding

First, we investigated the startup characteristics on the lowtemperature side (from room temperature to 100 °C) of methanation under the co-feeding of O<sub>2</sub> gas using Ru-based catalysts with support materials of CeO<sub>2</sub>, ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub>.

Figure 1 presents the CO<sub>2</sub> and O<sub>2</sub> conversions over various Ru-loaded catalysts under a raw-material gas feed with a composition of  $CO_2:H_2:O_2:N_2 = 10:50:5:35$ , using an online mass-spectrometry system. The reaction temperatures were set to room temperature, 50 °C, and 75 °C. The quartz tube was packed with 300 mg of catalyst (average particle size of 500  $\mu$ m $\phi$ ) and 400 mg of quartz sand, yielding a uniformly diluted catalyst layer. Prior to the reaction, the catalyst was reduced at 500 °C. In Figure 1, the horizontal axis indicates the time on stream, with the start of the feeding of the raw material as the zero point. For the Ru/CeO<sub>2</sub> catalyst at room temperature, CO<sub>2</sub> conversion increased sharply at the moment when the reaction gas was fed, reaching approximately 80% in <2 min. The product was mostly methane, and it was confirmed that AM was rapidly activated over this catalyst. Additionally, O<sub>2</sub> conversion reached 100% when the reaction gas was supplied. Because the product (methane) was not burned, it is considered that the hydrogen-oxygen combustion occurred rapidly and that AM proceeded by utilizing the combustion exothermic energy (Lewis and Elbe 1961; Fukuhara et al. 2020; Hirata et al. 2020). In contrast, the Ru/ZrO<sub>2</sub>, Ru/Al<sub>2</sub>O<sub>3</sub>, and Ru/SiO<sub>2</sub> catalysts did not exhibit methanation activity at room temperature, and AM rarely proceeded over these catalysts. There was no consumption of the supplied O<sub>2</sub>, and only a small amount of O<sub>2</sub> was consumed because of the oxidation of the catalyst after the supply of the raw-material gas. The methanation activity of the Ru/ZrO2 and Ru/Al2O3 catalysts on the low-temperature side was examined at the setting temperature of 50 °C. Although it was slower than that of the  $Ru/CeO_2$  catalyst, methanation started after >2 min over the  $Ru/ZrO_2$  catalyst and after  $\geq 5 min$  over the  $Ru/Al_2O_3$  catalyst. The  $O_2$  consumption increased rapidly to 100%. The hydrogen-oxygen combustion proceeded with the assistance of the heat energy at 50 °C (not a large amount) from the outside; thus, methanation successfully started over these catalysts. Over the Ru/SiO2 catalyst, methanation on the



Figure 1. Dynamic starting profiles of methanation (CO<sub>2</sub> and O<sub>2</sub> conversions) at (a), (b) room temperature, (c), (d) 50 °C, (e), (f) 75 °C using various Ru-based catalysts.

low-temperature side finally proceeded at the reaction temperature of 75 °C. Additionally,  $O_2$  conversion exhibited a slower rising behavior than those over other catalysts, and the combustion was slow. However, even over the Ru/SiO<sub>2</sub> catalyst, methanation started at a reaction temperature of 75 °C. This is a new finding that has not previously been reported.

It was inferred that one of the reasons for the difference in the activation characteristics of methanation under the  $O_2$ co-supply was the difference in the physicochemical properties of the different support materials. Table 1 presents the physicochemical properties of each catalyst. The Ru/SiO<sub>2</sub> catalyst had the largest specific surface area, followed by the Ru/Al<sub>2</sub>O<sub>3</sub> and Ru/CeO<sub>2</sub> catalysts. The Ru/ZrO<sub>2</sub> catalyst had

Table 1. Physicochemical property of varie	ous Ru-based catalysts.
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	B.E.T. surface area (m²/g-cat)	Amount of Ru (wt%)	Ru crystallite size <sup>a</sup> (nm)	Ru surface area <sup>b</sup> (m²/g)
Ru/CeO <sub>2</sub>	123	10	30.5	16.0
$Ru/ZrO_2$	90	9	8.8	55.2
$Ru/Al_2O_3$	134	11	48.0	10.2
Ru/SiO <sub>2</sub>	307	7	162	3.0

<sup>a</sup>Calculated using the Scherrer's equation.

<sup>b</sup>Estimated by CO-pulse method.

the smallest specific surface area. The amount of Ru loaded was approximately 10 wt% for the Ru/CeO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts and was slightly smaller for the Ru/ZrO<sub>2</sub> and Ru/SiO<sub>2</sub> catalysts. The amount of metal loaded via the

impregnation method appeared to be affected by the type of support material. The particle size of the supported Ru species was the smallest for the  $ZrO_2$  support; thus, the metal surface area was large. The Ru particle size was the largest for the SiO<sub>2</sub> support, and the metal surface area was small. The Ru species on the CeO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> supports were located between the two catalysts. The physical characteristics of the catalysts (such as B.E.T. surface area, Ru crystallite size and Ru surface area) were compared with the start state and performance characteristics of AM shown in Figure 1, and no clear correlation among them was observed.

#### 3.2 Factors affecting the startup of methanation

The factors affecting the methanation startup characteristics of each Ru-loaded catalyst under  $O_2$  co-supply were investigated.

Figure 2 shows the monitoring results for the temperature change of each catalyst layer when the CO<sub>2</sub>, H<sub>2</sub>, and O<sub>2</sub> gases were sequentially supplied to the catalyst layer and the order of the supplied gases was changed. The reaction temperature was 50 °C, and the supply conditions of the raw materials (gas composition and feeding rate) were identical to those of Figure 1. The temperatures at the inlet and outlet of the catalyst layer were measured by a data logger at intervals of 500 ms. In Figure 2, OP1 corresponds to the supply order of  $H_2 \rightarrow O_2 \rightarrow CO_2$ , OP2 corresponds to  $H_2 \rightarrow CO_2$  $\rightarrow$  O<sub>2</sub>, and OP3 corresponds to CO<sub>2</sub>  $\rightarrow$  H<sub>2</sub>  $\rightarrow$  O<sub>2</sub>. For the Ru/CeO<sub>2</sub> catalyst, the temperature of the catalyst layer increased immediately after the supply of the O2 gas in all cases. For OP1, the temperature was increased further by supplying the CO<sub>2</sub> gas after the temperature rise due to the supply of O<sub>2</sub>. This suggests that the hydrogen-oxygen combustion occurred first, and the subsequent supply of CO<sub>2</sub> proceeds the methanation. For OP2 and OP3, the temperature did not increase before the supply of O2 but after it, confirming the acceleration of methanation due to the hydrogen-oxygen combustion energy. Similar behavior was observed for the Ru/ZrO2 and Ru/Al2O3 catalysts. However, compared with the case of the Ru/CeO<sub>2</sub> catalyst, there was a time lag of several minutes before the temperature increased after O<sub>2</sub> supply. For OP1, time lags of 30 s for the Ru/ZrO<sub>2</sub> catalyst and 60 s for the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst were observed upon the temperature rise after O<sub>2</sub> supply. The hydrogenoxygen combustion on the catalyst was also affected by the type of support material. For OP2 and OP3 with the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts, the time lag was extended to approximately 120 s. In both operations, CO<sub>2</sub> was supplied before  $O_2$ . Therefore, it is considered that  $CO_2$ adsorbed on the catalyst surface inhibited the hydrogenoxygen combustion by forming the formate and formic acid species (Little 1971; Binet et al. 1999; Fukuhara et al. 2017). Because the order of the gas supply affects the reaction characteristics in this way, it is suggested that combustion and methanation proceed on the catalyst surface and that the physicochemical properties of the support materials affect the combustion performance.



Figure 2. Temperature profile changes of various Ru-based catalyst bed by changing fed order of methanation gas at 50  $^{\circ}$ C.

Figure 3 shows the XPS profiles of the support element, which were obtained via *in situ* XPS measurements for each Ru catalyst H<sub>2</sub>-reduced at 500 °C. In the curve-fitted profile of the CeO<sub>2</sub> support, peaks attributed to Ce<sup>3+</sup> and Ce<sup>4+</sup> were observed. It is known that oxygen defects are present on the surface of H<sub>2</sub>-reduced CeO<sub>2</sub> (Chen et al. 2009; Wang et al. 2016, 2017; Huang et al. 2018; Li et al. 2019; Zhu et al. 2020). Therefore, the peak attributed to Ce<sup>3+</sup> indicated that oxygen defects were present on the surface of the prepared Ru/CeO<sub>2</sub> catalyst. In contrast, for the ZrO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>



Figure 3. XPS spectra of (a) Ce3d of Ru/CeO<sub>2</sub>, (b) Zr 3d of Ru/ZrO<sub>2</sub> and (c) Al 2p of Ru/Al<sub>2</sub>O<sub>3</sub> catalysts.

supports, only Zr<sup>4+</sup> and Al<sup>3+</sup> peaks were observed, and there were no other valence elements. The Ru/ZrO2 and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts had no oxygen defects even on the H<sub>2</sub>reduced surface. It has been reported that  $Ce^{3+} - V_0^{"} - Ce^{3+}$  $(V_0^{"}: oxygen defect)$  species are present on the CeO<sub>2</sub> supports having such oxygen defects; O2 molecules are easily activated at this Vo" site, and H2 molecules are smoothly activated on Ce3+ (Chen et al. 2009; Huang et al. 2018; Li et al. 2019; Zhu et al. 2020). Thus, the combustion of  $H_2$ rapidly proceeds. In Figure 2, the fact that the combustion proceeded over the Ru/CeO2 catalyst almost at the same time as the supply of  $O_2$  confirms the relationship between the oxygen-defect site and the combustion property on the catalyst. The rapid starting of H<sub>2</sub> combustion allowed the progression of the AM phenomenon in the room-temperature region shown in Figure 1. However, because there were no oxygen defects on the Ru/ZrO2 or Ru/Al2O3 catalysts, which were the active sites of H<sub>2</sub> combustion, the supplied O<sub>2</sub> was adsorbed on the surface competitively with H<sub>2</sub> and CO<sub>2</sub> molecules. The absence of oxygen defects on both catalysts may be one of the reasons why it took time for the combustion to start after O2 was supplied for OP1 and why



Figure 4. CO<sub>2</sub>-TPD profiles of (a) various Ru-based catalysts and (b) support materials.

it took more time for OP2 and OP3, where  $CO_2$  was supplied before  $O_2$ .

Figure 4 shows the CO<sub>2</sub>-TPD profiles for each catalyst. After a reduction treatment at 500 °C, CO<sub>2</sub> was adsorbed on the catalyst surface under a supply of 1 vol% CO<sub>2</sub> (He balance) at 50 °C for 1 h. Subsequently, the signal of CO<sub>2</sub> (m/z = 44) was measured using a mass spectrometer while the temperature was increased from 20 to 850 °C at a rate of 10 °C/min under the supply of the He gas. Three peaks were observed for the Ru/CeO2 catalyst. The peak at approximately 100 °C corresponded to CO2 adsorbed on weak base sites, and that at 200-350 °C corresponded to CO<sub>2</sub> adsorbed on strong base sites (Luo et al. 1997; Wu et al. 2015; Zhang et al. 2016). The peak at 680–800 °C in the high-temperature range is attributed to CO<sub>2</sub> desorption over the catalyst with lattice oxygen. These peaks were observed in the same temperature range for the CeO<sub>2</sub> support alone, but the peak intensity at 200-350 °C increased when the Ru component was loaded. This temperature range coincides with the temperature range in which methanation activity is accelerated. The increase in the amount of CO<sub>2</sub> adsorbed is considered to be one of the reasons why the Ru/CeO<sub>2</sub> catalyst exhibited high methanation performance. The Ru/CeO<sub>2</sub> catalyst could adsorb CO<sub>2</sub> not only on the ruthenium element but also on the CeO<sub>2</sub> substrate (Binet et al. 1999; Chen et al. 2009; Panagiotopoulou et al. 2012; Akamaru et al. 2014; Aziz et al. 2015; Wang et al. 2016). Such dual gateways for CO<sub>2</sub> adsorption would bring about increment of adsorbing amount and acceleration of methanation process. The Ru/ZrO<sub>2</sub> catalyst and the ZrO<sub>2</sub> support differed from the Ru/CeO<sub>2</sub> catalyst in that only a large broad peak was observed from the low-temperature side to 300 °C. The Ru/Al<sub>2</sub>O<sub>3</sub> catalyst and the Al<sub>2</sub>O<sub>3</sub> support exhibited similar profiles. These large peaks corresponded to CO<sub>2</sub> adsorbed on weak or strong base sites on each catalyst (Luo et al. 1997; Bachiller-Baeza et al. 1998; Song et al. 2017; Quindimil et al. 2020). Such a difference in the adsorption state of CO<sub>2</sub> is related to the difference in the startup property of methanation in the presence of oxygen, as shown in Figures 1 and 2.

Figure 5 shows the profiles of  $H_2O$ -TPD for each catalyst. After the reduction treatment at 500 °C,  $H_2O$  was adsorbed on the catalyst by supplying 5 vol%  $H_2O$  (He balance) for 1 h at 50 °C. Then, the  $H_2O$  signal was measured using a TCD while the temperature was increased from 20 to 850 °C



Figure 5.  $H_2O$ -TPD profiles of (a) various Ru-based catalysts and (b) support materials.

at a rate of 10°C/min under He gas supply. The H<sub>2</sub>O desorption profiles of the Ru-supported catalysts were almost identical to that of the support alone. The largest amounts of H<sub>2</sub>O were desorbed for Ru/Al<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub>, followed by Ru/ZrO2 and ZrO2 and then Ru/CeO2 and CeO2. The fact that the Ru/CeO2 catalyst exhibited the smallest amount of H<sub>2</sub>O desorption is attributed to the rapid AM activation on this catalyst. In methanation, in the presence of oxygen, H<sub>2</sub> combustion first occurs over the catalyst, generating H<sub>2</sub>O. Because H<sub>2</sub>O is a product of methanation, it is preferable that the amount of H<sub>2</sub>O is small on the catalyst surface from the viewpoint of the thermodynamic theory. The amount of H<sub>2</sub>O generated over the Ru/CeO<sub>2</sub> catalyst was small, and the H<sub>2</sub>O was easily desorbed. This feature did not prevent the rapid AM activation over the Ru/CeO<sub>2</sub> catalyst. Conversely, the presence of a relatively large amount of H<sub>2</sub>O over the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts is considered to be one of the factors that make it difficult for the methanation to proceed.

## 3.3 Effects of feeding flow rate and O<sub>2</sub> concentration on AM

We previously reported that the AM phenomenon over the  $Ru/CeO_2$  catalyst is affected by the  $O_2$  concentration and the velocity of the gas supplied (Hirata et al. 2020). The same tendency was expected for the  $Ru/ZrO_2$  and  $Ru/Al_2O_3$  catalysts.

Figure 6 shows the effects of changes in the O<sub>2</sub> concentration and gas feeding rate on the AM properties for the Ru/CeO<sub>2</sub>, Ru/ZrO<sub>2</sub>, and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts. All results were obtained at room temperature without external heating. Considering that the AM phenomenon is related to the heat-generation state of the catalyst layer, to standardize the residence time of the supplied gas and to avoid the heat capacity of quartz sand (the diluent), each catalyst layer was set to have a width of 8 mm and a length of 10 mm with only each catalyst component. The packing amounts were 750, 600, and 325 mg for Ru/CeO2, Ru/ZrO2, and Ru/Al2O3, respectively. The composition of the raw-material gas was  $CO_2:H_2:O_2:N_2 = 10:42-60:1-10:47-20$  (N<sub>2</sub> balance). The flow rate of the gas was varied from 200 to 800 mL/min; thus, the GHSV for this condition varied from 24,000 to 96,000 h<sup>-1</sup>. In the case of 1 vol%  $O_2$  and the Ru/CeO<sub>2</sub> catalyst, the methanation did not start at any flow rate, but the inlet temperature increased to 50-100 °C. Then, methanation started at a supply rate of 300 mL/min at 2 vol% O2, and AM occurred at a higher O2 concentration and gas rate. CO<sub>2</sub> conversion and methane selectivity tended to decrease with the increasing O<sub>2</sub> concentration and gas rate, owing to the equilibrium restriction on the high-temperature side of methanation. The temperature of the reaction field increased as the O<sub>2</sub> concentration and gas rate increased, and a temperature range of ≥600 °C was confirmed. However, an excessive temperature rise causes the detonation phenomenon in the reaction field. Therefore, in CO<sub>2</sub> gas treatment by AM, it is important to select the O<sub>2</sub> concentration and gas supply rate that satisfy the treatment target. Over the



Figure 6. Relationship between auto-methanation property and reaction condition ( $O_2$  concentration and feeding flow rate). (a), (d), (e):  $CO_2$  conversion, (b), (e), (h):  $CH_4$  selectivity and (c), (f), (i): contour profile of inlet temperature (radial center).

Ru/ZrO<sub>2</sub> catalyst, at a concentration of  $\leq$ 3 vol% O<sub>2</sub>, methanation did not start at any gas supply rate, and the inlet temperature did not increase. The small amount of catalyst may have been responsible for this result. However, at  $\geq$ 4 vol% O<sub>2</sub>, methanation was activated at any gas supply rate, and AM in the room-temperature region progressed even over the Ru/ZrO<sub>2</sub> catalyst. This tendency was also observed for the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst, and the AM reaction started at  $\geq$ 4 vol% O<sub>2</sub> and  $\geq$ 300 mL/min. Thus, the Ru/CeO<sub>2</sub> catalyst was the easiest to activate, but the fact that AM in the room-temperature region also occurred over the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts implies a wide range for catalyst selection. Regarding the temperature profile of the catalyst layer, it appears that the Ru/ZrO<sub>2</sub> catalyst had many low regions and the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst had many

high regions compared with the  $Ru/CeO_2$  catalyst. Physicochemical properties such as heat capacity of the support materials may have contributed to this difference.

#### 3.4 Effects of H<sub>2</sub>-reduction temperature on AM

It is generally known that the reduction temperature of the catalyst affects its activity. Thus, the effect of the reduction temperature of the Ru-based catalyst on AM was investigated by changing the support materials.

Figure 7 shows the effect of the  $H_2$  reduction temperature on the starting state of AM with the Ru/CeO<sub>2</sub>, Ru/ZrO<sub>2</sub>, and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts. In all experiments, no external heating was performed during methanation. The catalyst layer



Figure 7. Effect of H<sub>2</sub>-reduction temperature on auto-methanation progression over each Ru-based catalyst.

was not diluted with quartz sand and had a diameter of 8 mm and a length of 10 mm, as in the case of Figure 6. The composition of the raw-material gas was  $CO_2:H_2:O_2:N_2 =$ 10:50:5:35, and the feeding rate was 400 mL/min. In the reduction operation, N2 was flowed at the time of the temperature rise, and the H<sub>2</sub> gas (flow rate 100 mL/min) was supplied for 1h after each reduction temperature was reached (from 50 to 500 °C). Then, the temperature was reduced to room temperature, and the raw-material gas was supplied after the state of the catalyst layer was stabilized. In the case of reduction at room temperature, only the  $H_2$  gas was supplied to the catalyst layer, without external heating. The Ru/CeO<sub>2</sub> catalyst exhibited a conversion of approximately 80% and a methane selectivity of approximately  $\geq$ 99.5% (a small amount of CO byproduct) at all reduction temperatures. Remarkably, it is a new discovery that the Ru/CeO<sub>2</sub> catalyst exhibited high AM performance with the reduction treatment in which H<sub>2</sub> alone was fed at room temperature, without external heating. The fact that such high AM activity was observed in the reduction treatment that did not require external heating energy confirms the superiority of the Ru/CeO<sub>2</sub> catalyst from the viewpoint of the economic efficiency of process operation. In contrast, the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts exhibited the AM activity with the reduction treatment in the presence of external heating energy. However, the Ru/ZrO<sub>2</sub> catalyst exhibited AM activity at a reduction temperature of  $\geq$ 75 °C, whereas the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst led to AM activity at a reduction temperature of  $\geq$ 150 °C, while maintaining a high performance of 70% to 80%. The advantage of the AM reaction conducted under oxygen supply is that the catalytic activity occurred even for the reduction treatment at temperatures of 75 and 150 °C and even over the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts.

Figure 8 shows the results of H<sub>2</sub>-TPR measurement for each Ru-based catalyst. The catalysts were oxidized at 300 °C for 1 h under O<sub>2</sub> gas flow and then cooled to -50 °C. After the catalyst bed became stable, the temperature was increased to 750 °C at 10 °C/min while feeding 4 vol% H<sub>2</sub>



Figure 8. H<sub>2</sub>-TPR profiles of various Ru-based catalysts.

 $(N_2 \text{ balance})$  at 50 mL/min. For the Ru/CeO<sub>2</sub> catalyst, a peak in the range of 20-70 °C and another in the range of 110-150 °C were observed. These peak profiles were clear. A weak broad peak over the range of 300-380 °C was also observed. The peak on the low-temperature side of 20-70 °C corresponded to the RuO<sub>x</sub> species, which were well-dispersed on the support, and the peak at 110-150 °C corresponded to the RuO<sub>x</sub> species, which aggregated in the bulk (Wang et al. 2009; Guo et al. 2018). The broad peak at 300-380 °C corresponded to the Ru species, which had a strong interaction with the support. For the Ru/ZrO<sub>2</sub> catalyst, the peak profiles could be divided into three temperature ranges. However, the peak in the lowest temperature range was shifted to 45-80 °C, and its intensity was low. Because the peak states of the other two temperature ranges were almost identical, it is suggested that the dispersibility of the RuO<sub>x</sub> species corresponding to the peak at 45-80 °C was lower than that of the Ru/CeO<sub>2</sub> catalyst. The peak profile obtained with the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst was shifted to the higher-

temperature side compared with those of the other two catalysts. The RuO<sub>x</sub> species on this catalyst were not well-dispersed, which was confirmed by scanning electron microscopy in a previous study (Fukuhara et al. 2020). The TPR results indicated that the prepared Ru-based catalyst contained RuO<sub>x</sub> species that were easily reduced on the lowtemperature side. The reduction-temperature range was of the following order:  $Ru/CeO_2 < Ru/ZrO_2 < Ru/Al_2O_3$ . This order is consistent with the AM startability trend shown in Figure 7. The Ru species on the Ru/CeO<sub>2</sub> catalyst formed metallic Ru even under H<sub>2</sub> reduction in the room-temperature region without external heating and served as active sites whereat AM progressed. In contrast, the Ru species on the Ru/ZrO<sub>2</sub> catalyst were not reduced by H<sub>2</sub> reduction in the room-temperature region; the metal Ru species were formed at 75 °C, and the AM proceeded. Similarly, the Ru species on the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst must be reduced at a higher temperature than those on the Ru/CeO2 and Ru/ZrO<sub>2</sub> catalysts, and the H<sub>2</sub>-reduction treatment at 150 °C promoted AM. It is considered that the difference in the reducing characteristics of the RuOx species due to the difference in the support materials was related to the AM activity.

In situ XPS measurements of each catalyst were performed to investigate the electronic states of the Ru species on the support. Figure 9 shows profiles of the Ru species of the Ru/CeO<sub>2</sub>, Ru/ZrO<sub>2</sub>, and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts treated at different reduction temperatures. In the catalyst, before reduction (as made), peaks attributed to Ru<sup>4+</sup> and Ru<sup>n+</sup> (0 < n < 4) were observed for all supports (Elmasides et al. 1999; Chakroune et al. 2005; Yuan et al. 2015; Ma et al. 2017; Hu et al. 2018). The peak profiles were affected by the H<sub>2</sub>-reduction treatment, that is, by the reduction temperature. The profiles also depended on the support type. For the Ru/CeO<sub>2</sub> catalyst, a peak of 280 eV belonging to Ru<sup>o</sup> species was confirmed by the reduction treatment in the room-temperature region, which corresponded to the peak on the low-temperature side shown in Figure 8 for H<sub>2</sub>-TPR. As the reduction temperature increased, the intensity of the peak belonging to the Ru<sup>o</sup> species increased, and the intensity of the peak of the Ru4+ species decreased. At a reduction temperature of 500 °C, the peak of the Ru<sup>o</sup> species was dominant. For the Ru/ZrO<sub>2</sub> catalyst, the peak of the Ru° species was not observed at reduction temperatures of  $\leq$ 50 °C but was observed at  $\geq$ 100 °C. Similarly, for the Ru/Al<sub>2</sub>O<sub>3</sub> catalyst, Ru<sup>o</sup> species were not detected at reduction temperatures of  $\leq$ 50 °C but were detected at  $\geq$ 100 °C. These results are consistent with the AM progression over the Ru/CeO<sub>2</sub> catalyst with a low reduction temperature, as shown in Figure 7. The easy-reduction property of the Ru/CeO<sub>2</sub> catalyst in the room-temperature region may be related to physicochemical properties, such as oxygen defects and CO<sub>2</sub>- and H<sub>2</sub>O-adsorption properties. This can be investigated in a future study.

#### 4. Conclusions

The AM reaction over various Ru-based catalysts with different support materials positively proceeded by selecting the reaction conditions, such as  $O_2$  concentration and gas flow rate. The Ru/CeO<sub>2</sub> catalyst exhibited the highest catalytic activity, followed by the Ru/ZrO<sub>2</sub> and Ru/Al<sub>2</sub>O<sub>3</sub> catalysts. The progression of AM over the Ru/SiO<sub>2</sub> catalyst was slow. As well as to the difference in adsorption characteristics between CO<sub>2</sub> and H<sub>2</sub>O, the rapid progress of AM over the Ru/CeO<sub>2</sub> catalyst was attributed to the oxygen defects



Figure 9. XPS spectra of Ru element for (a)  $Ru/CeO_2$ , (b)  $Ru/ZrO_2$  and (c)  $Ru/Al_2O_3$  catalysts with different  $H_2$ -reduction temperature.

 $(Ce^{3+}-V_0^{"}-Ce^{3+})$  species on the CeO<sub>2</sub> supports that accelerated the hydrogen-oxygen combustion; O<sub>2</sub> molecules are easily activated at this V<sub>O</sub><sup>"</sup> site, and H<sub>2</sub> molecules are smoothly activated on Ce<sup>3+</sup>. AM proceeded over each Rubased catalyst even when the catalyst was H<sub>2</sub>-reduced at a low temperature. The Ru/CeO<sub>2</sub> catalyst was advantageous over the other catalysts because the AM proceeded under the supply of the H<sub>2</sub> gas alone in the room-temperature region without external heating. XPS results indicated that metal Ru species were formed on the Ru/CeO<sub>2</sub> catalyst by H<sub>2</sub> reduction in the room-temperature region and were associated with the progression of AM. The progress of methanation by H<sub>2</sub> reduction at such a low temperature strengthens the CO<sub>2</sub> conversion process.

## **Disclosure statement**

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