

Abstract. Optical fibre probing is widely applied to measurement in gas-inquid two-phase flows. We already developed and reported a Four-Tip Optical fibre Probe (F-TOP) for millimetre-size bubbles/droplets, and a Single-Tip Optical fibre Probe (S-TOP equipped with a wedge-shaped tip) for sub-millimetre-size bubbles/droplets. However, it is difficult to measure micrometre-size bubbles/droplets by S-TOP. The main purpose of the present study was to develop a new type of optical fibre probe micro-fabricated by a femtosecond pulse laser (fs-ProbeFs-TOP). First, we confirmed the performance of the new probe by examining millimetre- and sub-millimetre-size droplets; the results by fs-ProbeFs-TOP were compared with those obtained from the visualization of the droplets by high-speed video camera, and showed satisfactory agreement. In addition, we demonstrated the measurement of velocities and chord lengths of micrometre-size droplets (about 50 µm in diameter) using the fs-ProbeFs-



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bubbles via by optical fibre probe, a multi-tip probe is not applicable, because the multi-tip optical fibre probe is too large to surely pierce such spheresthem. In order to solve this problem, the authors developed a Single-Tip Optical-fibre Probe (S-TOP) which realizes the simultaneous measurement of chord lengths and velocities of tiny bubbles/droplets at low velocities (Saito 1999, 2002). However, it-this probe is difficult tocannot measure micro droplets/bubbles at high velocities by the S-TOP owing tobecause of its measurement principle. To break throughovercome this problem, we have developed a new type of optical fibre probe micro-fabricated by femtosecond pulse laser (fs-ProbeFs-TOP), which realizes simultaneous measurement of chord lengths and velocities of tiny droplets/bubbles at high velocities.

The S-TOP and fs-ProbeFs-TOP have the distinguished properties compared with the other former probes. Each optical probe hashave different kinds of characteristics; therefore, they should be used underselected with careful consideration of their application ranges reflecting their characteristics. In the present paper, those characteristics and the comparisons of them are described and compared. B based on the comparisons between correlation of the measurement results of each of the S-TOP/fs-Probe and with those of visualization, we consider their characteristics and compare their performance as follows.

In addition, we propose various methods for interpreting the results. In a single probe method,* the probe should pierce the centre region of a droplet/bubble in order to accurately measure its minor axis. First, we propose aOur newly developed method using a pre-signal to-can detect whether the S-TOP/fs-ProbeFs-TOP has pierceds the centre region of a droplet/bubble. Second, wWe also discuss the forced deformation when the probe touches the droplet interface. Focusing on _ and its relation to droplet's size and velocity, we discuss this deformation. Third, wWe carefully discuss the influences of the droplet another deformation taking place of the droplet during the S-TOP/fs Probe measurement (i.e. ; namely, that while the probe is piercing the dropleit, on the measurement results). Based on these theoretical discussions, we describe interpret the actual results of millimetre-size and sub-millimetre-size 600 µm, sub-mm-size) droplet droplet-measurements via-by S-TOP and fs-ProbeFs-(300)TOP. We confirm the performance and properties of the S-TOP/fs Probe by examining millimetre droplets, sub-millimetre-size droplet (sub-mm-size droplet). In addition, we

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2.1 Single-Tip Optical fibre Probe (S-TOP) and new type of optical fibre probe (fs-ProbeFs-



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2.1.1 S-TOP. Figure 1 shows the structure of the S-TOP used in the present study. The S-TOP was made of a synthetic silica optical fibre (<u>external diameter</u>, 230μm; <u>core diameter</u>, <u>in</u> external diameter, 190μm in core diameter, jacket thickness, 15μm; refractive index in jacket thickness, 1.46 in refractive index</u>). The silica optical fibre was fine-drawn using a micropipette puller (P-2000, Sutter Instrument Company). After that, the tip was ground in <u>at</u> an angle of 30 degrees with to the fibre axis via by a micropipette beveller (BV-10, Sutter Instrument Company); the most distinguishable feature of the S-TOP is that its tip is ground

in-<u>at</u> an angle of 30 degrees <u>with-to</u> the fibre axis. The tip diameter is 20µm. This fibre was inserted and fixed in a stainless capillary. Accordingly, chord lengths and velocities of bubbles/droplets are measured using only a single_-tip optical fibre probe. Furthermore, S-TOP is coated with <u>a</u> water repellent material by vacuum evaporation of a water repellent material in order to control the surface wettability.

2.1.2 <u>fs-ProbeFs-TOP</u>. Figure 2 shows the structure of the <u>fs-ProbeFs-TOP</u> used in the present study. The <u>fs-ProbeFs-TOP</u> was made of a synthetic silica optical fibre (<u>external diameter</u>, 230µm; <u>core diameter-in external diameter</u>, 190µm; <u>jacket thickness</u>, <u>in core diameter</u>, 15µm; <u>refractive index, in jacket thickness</u>, 1.46-in refractive index). The silica optical fibre was also fine-drawn using the micropipette puller. After that, the clad near the tip was processed by femtosecond pulses. A close-up picture is shown in Figfigure. 2. Since a clad is stripped from a core at the groove, the core touches <u>the</u> air directly. The phase detection is done in two stages (i.e. at tip of the probe and at the groove). This fibre was inserted and fixed in a stainless capillary. <u>TFurthermore</u>, the <u>fs-ProbeFs-TOP</u> is <u>also</u>_coated with water repellent material by vacuum evaporation of a water repellent material.

2.2 Rational targets for S-TOP and *fs-ProbeFs-TOP* measurements.

The S-TOP and <u>fs-ProbeFs-TOP</u> have the <u>distinguished_distinguishing_properties</u> compared[•] with <u>the other</u>-conventional probes. Furthermore, our probes have different characteristics owing to <u>the differences in their of</u>-measurement principles and manufacturing processes. The S-TOP can be made very easily; the tip of the S-TOP is only micro-ground into a wedge shape. Hence, the wedge-shaped tip is gradually covered with the <u>other opposite</u> phase (liquid phase in the cases of <u>the</u>-droplet measurement; <u>_______</u> gas phase in the cases of <u>the</u>-bubble measurement). By contrast, <u>m</u>Micro-fabrication of <u>the fs-ProbeFs-TOP</u> needs-requires a high-power femtosecond-pulse laser, nano-order 6-axes automatic optical stages, confocal optics, and so on. <u>The fabricationIt</u> is very difficult to <u>make_fabricate</u> the <u>fs-ProbeFs-TOP</u> with <u>the</u> desired performance.

It is important to use intelligently both-select between these two probes due-according to the measurement objective, based on a thorough understanding of their properties.

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Matsuda & Saito MST/307768 -

Figure 3 shows the <u>a</u> schematic diagram of <u>the</u> measurement processes by using the S-TOP⁴ and <u>fs ProbeFs-TOP</u>. The S-TOP measures the velocities of bubbles/droplets by <u>a</u> very small tip. Hence, the S-TOP needs the <u>a</u> fast A/D converter and fast amplifier for the measurements of tiny bubbles/droplets moving at high velocity. This is a disadvantage of S-TOP measurement. Therefore, the measurement object of the S-TOP is the sub-mm-size droplet moving <u>at</u> less than several m/s.

On the other hand, the measurement object of the fs-ProbeFs-TOP is the um-size microdroplets and sub-mm-size droplets moving at over-10 m/s or more. The fs probeFs-TOP uses the signal from the probe tip and that from the groove. Hence, the time interval of the event time becomes larger than that of the S-TOP.

The S-TOP and <u>fs-ProbeFs-TOP</u> have <u>the</u> different application ranges, respectively. In this paper, we confirm the performance of the <u>fs-ProbeFs-TOP</u> and S-TOP by examining millimetre- and sub-mm-size droplets for the first time. When the droplet velocity is around 10 m/s, the <u>fs-ProbeFs-TOP</u> can <u>highly accurately</u> measure the droplet property <u>with higher</u> accuracy compared with than the S-TOP.

2.3 Optics and data acquisition.

The optics <u>system</u> is shown in Fig.figure 4. The beam from a laser diode (a) (wavelength⁴ 635nm) is split by <u>a</u> beamsplitter (b), and focused on the fibre edge (d) by <u>an</u> objective lens (c). A p Part of the laser beam propagated through the optical fibre is reflected at the other tip (sensing side) of the optical fibre probe, changed its own polarization plane at the reflection and propagated back again through the same fibre; then it is input into a photo multiplier (f) through a polarizer (e) cutting the laser beam (i.e. the beam from the laser diode) with a different polarization plane from that of the reflected beam.Part of the laser beam propagated through the optical fibre is reflected at the other tip (sensing side) of the optical fibre probe, and propagated back again through the same fibre; then it was <u>is</u> input into a photo multiplier (f) through a polarizer (e) cutting a direct laser beam from the laser diode.

The optical signal was converted into an electrical signal viaby the photo multiplier (f). The electrical signal was stored in <u>a</u> digital oscilloscope (g) (sampling rate 200 MHz).

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2.3 Experimental setups.

Figure 4. Optics.

Figure 5 shows a schematic diagram of the experimental setup used in demonstration of millimetre-size droplet (droplet diameter: $1 \text{ mm} \le L_D \le 5 \text{ mm}$;) measurement by Fs-TOP and S-TOP. Droplets are launched from a micro capillary (h) (780 µm in inner diameter) placed over the probe (a). The equivalent diameter of the droplets is 2 mm, and their velocities varied between 0.25 m/s and 2.5m/s. We visualized the process of the droplets being pierced by the S-TOP using a high-speed video camera (e) (frame rate, 2900 fps; exposure time, 50 µs; resolution, 800×512 pixel²; and spatial resolution, 21.97 µm/pixel) and a halogen light (g).



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(a) Probe, (b) Optical stages, (c) Optics, -(d) Recorder, (e) Highspeed video camera, (f) PC, (g) Halogen light, (h) Needle, (i) Droplet Figure 5. Experimental

the experimental setup.used in Optical stages, (c) Optics, (d) Recorder, (e) High speed demonstration of millimetre size droplets (droplet diameter: $1 \text{ mm} \leq L_D \leq 5 \text{ mm}$;) measurement via by fs-Probe and S-TOP. Droplets are launched from a micro capillary (h) (780 µm in inner diameter) placed over the probe (a). The equivalent diameter of the droplets is 2 mm, and their velocities were varied between 0.25 m/s and 2.5m/s. We visualized the process of the droplets being pierced with by the S-TOP using a high speed video camera (e) (frame rate, 2900 fps, ; exposure time, 50 μ s, <u>resolution</u> 800×512 pixel², and

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halogen light (g).

Figure 6 shows a schematic diagram of the experimental setup used in experiments of sub-⁴ mm-size droplets (droplet diameter: 150 μ m $\leq L_D \leq$ 500 μ m; droplet velocity: 5 m/s $\leq U_D \leq$ 25 m/s) measurement viaby fs-ProbeFs-TOP and S-TOP. Ion-exchange water in the a water tank (b) is-was pressurized by air (a) (gauge pressure 25 kPa $\leq P \leq$ 300 kPa), and the pressurized water was ejected from the nozzle (nozzle diameter D = 30, 60, 100, 150, 200 μ m) (e). The dDiameters of the droplets is-varied between 150 μ m and 500 μ m, and their velocity was varied between 5 m/s and 25 m/s. The probe was mounted on a three-degree-of-freedom precision micro stage (h) driven by micro stepping motors. The probe position was adjusted precisely using the micro stage a sthe probe was able to strike the <u>um-size-micro</u> droplets. The process of the piercing of droplets with the probe was also visualized using two high-speed video cameras (j) (frame rate 250000, 500000, 1000000 fps; exposure time 0.5 μ s, resolution 260×312 pixels², and spatial resolution 6.67 μ m/pixel) (k), and a strobe light (l) and a halogen light (m).

Figure 7 shows the schematic diagram of the experimental setup which used in the experiments of <u>um-size-micro</u> droplets measurement <u>via by fs ProbeFs-TOP</u>. Micrometer-size droplets (droplet diameter: $L_D \approx 30 \ \mu$ m, droplet velocity; 1.5 m/s $\leq U_D \leq 2.5 \ m$ /s) is-were ejected from the <u>a</u> piezoelectric ink jet nozzle (h). We visualized the contact process between the droplets and the <u>fs-ProbeFs-TOP</u> by-using a Hhigh-speed video camera (e) and a <u>sS</u>trobe light (g).



(a) Pressurization source, (b) Water tank, (c) Pressure controller, (d) Electromagnetic valve, (e) Piezo nozzle, (f) Digital oscilloscope, (g) Optical system, (h) 3-axis unit, (i) S-TOP, (j) High-speed video camera 1, (k) High-speed video camera 2, (l) Strobe light, (m) Halogen light source.
 Figure 6. Experimental setup for measurement of sub-millimetre-size droplets.

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Droplet,

(j) Controller, (k) Monitor, (l) Water tank

3. SIGNAL PROCESSING

3.1 Signal processing for S-TOP.

Matsuda & Saito MST/307768

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3.1.1 Characteristics of S-TOP signals. A typical signal in droplet measurements via-by the S-TOP is plotted in figureFig. 8. The wedge-shaped tip of the S-TOP is gradually covered with the other phase;-in consequently,ee the intensity of the light reflected at the tip is gradually changed (marked in figureFig. 8); the interface velocity is proportional to the derivative of the optical signal (derivative of the leading edge of optical signal) with respect to time (Saito 2007a, b). Therefore, mMeasuring the surface tension and viscosity of measurement objects preliminarily, a-the gas-liquid interface velocity is easily calculated by-using this relation (e.g. Saito *et al*_2000, Saito 2007c). Accordingly, chord lengths and velocities of bubbles/droplets are-were measured using only a single_-tip optical fibre probe. The gradient of a-the leading edge g_{rd} is calculated by equation (1),

$$\underline{g_{rd}} = \frac{dV}{-dt} \times \frac{1}{(V_{Gas} = -V_{Lianid})},$$
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where dV/dt is obtained from a burst signal, and the gas-phase output level V_{Gas} and liquidphase level V_{Liquid} are calculated as described in section 3.1.2. In a similar way, the gradient of the rising edge is calculated by the equation (1). DThe droplet velocity U_D (in a strict sense, the average interface velocity of a droplet) is calculated from equation (2)

$$U_{D} = \frac{1}{\alpha} \times g_{rd},$$
(2)

where α is the proportionality coefficient between the interface velocity and g_{rd} . The coefficient " α " depends on only 3 factors as follows: the angle of the S-TOP tip, the wettability between the probe and the liquid phase, and the surface tension of the liquid phase. The angle of the S-TOP tip is decided based on the results of ray trace calculation considering the difference of in refraction indexes between the core of the optical fibre and the liquid phase. After that, the value of the coefficient " α " is decided by only the properties

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of <u>the</u> liquid phase (the wettability and surface tension). In this paper, these properties do not change, because we measure only water droplets.

Figure <u>89</u> shows the relationship between g_{rd} obtained by S-TOP measurements and U_D by visualization. As shown in this figure, the value of the coefficient " α " of <u>the</u> calculated value 5.60x10⁻⁶ is adequate.

The chord length L_D is calculated from equation (3),

 $L_D = U_D \times (t_e - t_s), \qquad (3)$

where t_s and t_e are the starting and finishing-end times of contact between the S-TOP and the droplet. The event time t_s is defined as an intersection point of the straight line (i.e. the gradient is g_{rd}) and the gas_phase level at the leading edge. The event time t_e is defined as an the intersection point of the straight line (i.e., the gradient is g_e) and the liquid_phase level at the rising edge.

3.1.2 Evaluation of droplet deformation and Pre-signal. Figure 10 shows schematic drawings⁴ of <u>the</u> S-TOP/<u>fs ProbeFs-TOP</u> measurement. When the probe pierces the centre region of a droplet/bubble, the <u>ch</u>ord length obtained <u>via_by</u> probe is very similar to the droplet's/bubble's minor axis. In the measurements of droplets/bubbles, <u>Hfif</u> L_{Ml} is limited within an area of $L_{Ml} / L_{Bl} < 0.3$, i.e. within the centre region, the difference between the measured chord length L_M and the length of the minor axis of a droplet/bubble L_{Ds} is small (0.95 < $L_{Ms} / L_{Bs} < 1.00$). When the probe pierces droplets/bubbles in the centre region, highly accurate measurement is achieved. In addition, the small difference between the minor-axis and measured chord lengths is a kind of random difference; therefore, it is very difficult to remove it-them from the measurement results.



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| $>$ Sub-mm-size droplets ($L_D = 250 \pm 60 \ \mu m$) |
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| Sub-mm-size droplets ($L_D = 300 \pm 60 \ \mu m$) |
| \odot Sub-mm-size droplets ($L_D = 500 \pm 60 \ \mu m$) |
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Figure 11 shows snapshots that in which the fs-ProbeFs-TOP touches, on the one hand, the a flat interface and on the other, a sub-mm-size droplet. In the cases of touching the flat interface at low velocity (a-the velocity of the probe is 100 mm/s), a large deformation is observed on at the gas-liquid interface as shown in figureFig. 11 (a). On the other hand, when the fs-ProbeFs-TOP touches a sub-mm-size droplet at a high velocity (10 m/s), the deformation of the droplet is very small as shown in figureFig. 11 (b). Hence, the deformation of the droplet does not become a serious problem when we measure measuring tiny droplets moving at a high velocity. Unfortunately, this deformation is was not measured quantitatively. The deformation of the droplet while pierced by the probe is very small during measurement (between t_s and t_e), as shown in the snapshots of figure Fig. 8. In the case of sub-mm-size droplet measurements, the deformation is smaller than 3.2 % of droplets' minor axes (this difference is a kind of bias), and in the case of <u>um-size micro-size</u> droplet measurement it is smaller than 3.1 % of the droplets' minor axes (this difference is a kind of bias); i.e., the measurement is completed before large deformation. In fact, as the probe pierces the droplet in this region, highly accurate measurement is achieved. However, we need to know how to detect the pierced position by of piercing using the single-tip optical fibre probe, to ensure that the probe has pierced the centre of the droplet.



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(a) Snapshots: The fs-Probe touching the <u>a</u> flat interface at <u>a</u> low velocity (100 mm/s); the fs-Probe touches the interface just at t = 0 [ms].



(b) <u>Snapshots:</u> The fs-Probe touching a sub-mm<u>-size</u> droplet moving at a high velocity (10m/s);

Figure 11. Snapshots of touching process under different conditions.

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We found out that a pre-signal appears only when the wedge-shape tip of the botheither probe[•] (equipped with wedge shape tip) pierces the centre region of a droplet/bubble. In the case of bubble measurement, most beams are emitted from the probe tip before they pierce a-the bubble, because the probe tip is covered withsurrounded by _-liquid phase before the detectionencountering of the bubble. Hence, the emitted beams are reflected on the bubble frontal surface, and some of them re-enter into the probe; this these incident beams are serve as a pre-signal. On the other hand, in the droplet measurement, few beams are emitted from the probe tip, because the probe tip is covered withsurrounded by gas phase before the detection of encountering the droplet. Therefore, the no pre-signal does not appears before the detection of the droplet. However, the a pre-signal similar to the pre-signal of the bubble measurement appears just before the probe pierces the rear interface of the droplet only when the probe pierces the centre region.

In the measurement by using a single tip probe, this measurement method realizes the highaccuracy measurement of the minor axes of the bubbles and droplets. **書式変更:**両端揃え

Matsuda & Saito MST/307768

3.1.3 Algorithsm for S-TOP. Figure 12 shows the algorithsm for the processing of S-TOP⁴ signals. The signal processing is composed of four processes as described herein-below; 1) the sSmoothing process, 2) the dDetermination of thresholds, 3) the D detection of event time and gradient of a-the burst signal, and 4) the cC alculation of chord length and velocity.

1) Smoothing process

The raw data of output signals are smoothed viaby <u>a</u>_25-point moving average method to⁴ reduce the influence of high-frequency noise.

2) Determination of thresholds

We use the thresholds to accurately detect the event time. First, the maximum output voltage V_{max} and the minimum output voltage V_{min} are detected. Second, V_{Gas} and V_{Liquid} are calculated. In this study, V_{Gas} is the average value of the voltage over 90 %, and V_{Liquid} is the averaged value of the voltage under 10 %. Finally, the high threshold level V_{thh} and the low threshold level V_{thl} are decided. In this study, the high threshold level V_{thh} was 90 % of all-the entire signal amplitude, and the low threshold level V_{thl} was 30 % of all-the entire signal amplitude. These threshold values are decided by the results of comparison between the visualization and the probe signal. As a result, the difference of in detection of event time between the results of visualization and signal processing is less than 5% in all measurement cases. We consider this difference is as a kind of a bias difference (not random difference) in the calculation of event time; therefore, this bias is could be removed from the S-TOP measurement results.

3) Detection of event time and gradient of a burst signal

In this process, we detect the t_s at and t_e , and calculate the gradient of the signal. First, the gradient of the falling edge and rising edge is calculated by equation (1), as shown in section 3.1.1. Next_a we detect the duration time between the probe and <u>a-the</u> droplet. The event time t_s is defined as <u>an-the</u> intersection point of the straight line (i.e. the gradient is g_{rd}) and the gas_phase level at <u>the</u> falling edge. The event time t_e is defined as <u>an-the</u> intersection point of the straight line (i.e. the gradient is g_{rd}) and the gas_phase level at <u>the</u> falling edge. The event time t_e is defined as <u>an-the</u> intersection point of the straight line (i.e. the gradient is g_e) and the liquid_-phase level at <u>the</u> rising edge. As a result,

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we can calculate the event time. The bias (i.e. the difference is less than 5 % of the results via by visualization) is considered in the calculation.

4) Calculation of chord length and velocity

Finally, we calculate the droplet velocity and its chord length. In the calculation, we judge the piercinged position. First, we calculate the droplet velocity by equation (2) as shown in section 3.1.1. The chord length L_D is calculated from equation (3) (shown in section 3.1.1). Next, we estimate the time range of generation of the pre-signal from droplet velocity and its diameter. We search for the pre-signal in this range-by using a threshold. As part of this process, we can judge whether the probe pierces in the centre part of the droplet. Since When the probe pierces the centre part of a-the_droplet, we can measure the minor axes of the droplets. The pre-signal is described at-in detail in section 3.1.2.

3.1.4 The algorithsm for fs-ProbeFs-TOP. As shown in figureFig. 13, the signal processing is composed of five processes as described below: 1) the sSmoothing process, 2) the hHistogram process, 3) the dDetermination of thresholds, 4) the dDetection of event time and gradient of signal, and 5) the cCalculation of chord length and velocity.



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in 2nd process: "The maximum voltage" \rightarrow "The" should not be capitalized; "low threshold level" should be "lower threshold" and "high threshold" should be "upper threshold". In 3rd process "start time" is better than "starting time", don't use "a" before droplet or "the" before probe in "between probe and droplet" In 4th process, don't use "the" before U and L; use present tense "if pre signal is detected"

Fig. 4: The typical S-TOP signal and snapshots corresponding to the signal showing the contact process between a sub-mm-sized droplet and the S-TOP probe.

1) Smoothing process

The raw data of the output signals are smoothed viaby the 25-point moving average method to reduce the influence of high-frequency noise.

2) Histogram process

The histogram method (Sakamoto and Saito) is employed to accurately detect the output voltage levels.

Matsuda & Saito MST/307768 - - -

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We obtain the <u>a</u> histogram of <u>the</u> output voltage signal. The threshold values <u>which that</u> we want can be easily extracted from peak values of the histogram. Figure 14 shows an example of the histogram of <u>fs-ProbeFs-TOP</u> signals. <u>Clear fF</u>our <u>clear</u> peaks (marked in the figure) are detected from the histogram. Each peak corresponds to <u>the <u>a</u> stable output voltage level of <u>the fs-ProbeFs-TOP</u> signal:</u>

(1) Full gas_phase level (both probe tip and groove are positioned in air) = V_{Gas} ,

(2) Tip level (only the probe tip is positioned in the droplet) = V_{tl} ,

(3) Full <u>l</u>-iquid_-phase level (both of the probe tip and the groove are covered with<u>in</u> the droplet) = V_{Liquid} ,

(4) Groove level (the groove <u>is</u> in the droplet) = V_{gl} .

3) The determination of thresholds

We use the thresholds to accurately detect the event time in each level as shown in figureFig. 145. We decide the upper (V_{thl}) and lower (V_{thl}) first threshold levels to detect determine the startting time of contact between the fs ProbeFs-TOP and a droplet. The first high threshold level V_{thhl} and the first low threshold level V_{thll} are decided. In this study, V_{thhl} was 90 %, and V_{thll} was 30 % of the difference in the signal amplitude between V_{Gas} and V_{tl} . Next, the upper (V_{thh2}) and lower (V_{thl2}) second threshold levels are determined in order to detect the time the droplet touches the groove edge; here, the upper threshold level V_{thh2} was 90 %, and the lower threshold level V_{thl2} was 20 % of the signal amplitude between V_{liquid} and V_{tl} . Finally, the upper (V_{thb3}) and lower (V_{thb3}) third threshold levels are determined in order to detect the end time of contact between the fs-ProbeFs-TOP and the droplet; here, the V_{1hh3} was 90 %, and V_{thl3} was 20 % of the signal amplitude between V_{liquid} and V_{gl}. The second threshold level is decided in order to detect the time of the droplet touching the groove edge. The second high threshold level Vthh2 and the second low threshold level Vthl2 are decided. The high threshold level Vthh2 was 90 %, and the low threshold level Vthl2 was 20 % of signal amplitude between the Vliquid and Vtl. Finally, the third threshold level is decided in order to detect the finishing time of contact between the fs Probe and the droplet. The third high threshold level Vthh3 and the third low threshold level Vthl3 are decided.

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コメント [KN12]: Is this what you mean? Otherwise, I don't understand "signal amplitude between..."

コメント [KN13]: See above.

コメント [KN14]: See above.

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2nd-process: "Liquid" should not be capitalized, also don't need the paragraphing in that box. 3rd process: suggest "upper" instead of "high" threshold and "lower" for "low"; 4th process: suggest "start time" and "end time"; 5th process: delete "a" from the phrases "droplet velocity", "droplet chord length"; delete "the" from "the U"

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 V_{thh3} was 90 %, and V_{thl3} was 20 % of signal amplitude between the V_{liquid} and V_{el} . The difference of in detection of event time between the results of visualization and this signal processing is was less than 5.5 % in all measurement cases. We consider this difference in the calculation of the event time is as a kind of a bias difference (not a random difference); therefore, this bias is could be removed from the measurement results viaby fs Probe Fs-TOP.





Figure 15. Schematic diagram of signal processing for fs-Probe.

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In a similar way, the gradient of the second falling edge g_{rd2} (between V_{liquid} and V_{tl}) and the rising edge g_e (between V_{liquid} and V_{gl}) is calculated by equation (4). Next_a we detect the contact time between the probe and the droplet. We define t_s and t_e as the beginning start and finishing end times of contact between the fs Probe tip and the droplet. The t_{s2} is defined as the time when the droplet touches the groove edge. The t_{s2} is defined as time of the droplet touching the groove edge. The event time t_s is defined as an the intersection point of the straight line (i.e. the gradient is g_{rd}) and the gradient is g_{rd2}) and the gas_phase level at the first falling edge. An The intersection point of the straight line (i.e. the gradient is g_{rd2}) and the gradient is g_{rd2} and the liquid_phase level at the rising edge. As a result, we can detect event time in-with high accuracy (the difference is less than 5.5 % as described in the above).

5) Calculation of chord length and velocity

Finally, we calculate the droplet velocity and its chord length, and we judge the pierced position <u>of piercing</u> by the probe based on the pre-signal. First, we calculate the droplet velocity by equation $(5)_{\frac{1}{2}}$;

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where L_P is <u>a</u>-the distance between the tip point and the groove. The chord length L_D is calculated from equation (6),

 $L_D = U_D \times (t_e - t_s).$ (6)

Next, we judge whether the probe pierces in the centre part of the droplet by using the presignal (the algorithm is described in section 3.1.3, and the pre-signal is described in section 3.1.2).

4. Results and Discussion

4.1 The S-TOP measurements.

4.1.1 Characteristics of the S-TOP signals. The output signals in the S-TOP measurements of various diameter droplets are shown in figureFig. 16. When the sub-mm-size droplet contacts with the S-TOP, the output signal corresponding with the liquid_-phase level does not stabilize. Since the S-TOP diameter is inadequate in comparison with the droplet diameter, the smallest output becomes large with a decrease in the droplet diameter. Hence, the liquid does not cover surround the sensor section of S-TOP completely. Therefore, the output voltage corresponding with to the liquid-phase tends to be high when the droplet diameter is small. The typical output signals of the S-TOP and the corresponding pictures during its-the penetration process are shown in figureFig. 17. In figureFig. 17 (a), the output signal changes in two stages for successional penetration of two droplets. The output voltage of the S-TOP signal decreases with the penetration of the first droplet. Before the signal is restored to the gas-phase level, the signal again decreases due to the penetration of the next droplet. Therefore, the output voltage of the S-TOP decreases from the liquid_-phase level of the precedent-preceding droplet. We consider that this phenomenon is caused by a liquid-phase thin film which is formed on the S-TOP surface when the first droplet hits the S-TOP. Then The next droplet hits the S-TOP before the removal of the liquid thin film. In addition, in these measurements the amplifier frequency of the photo-multiplier is 20 kHz. This frequency

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is too low to detect a pre-signal i_{3} therefore no pre-signal is observed in the sample signals in <u>figureFig.</u> 17 (in order to detect a pre-signal, a frequency of 200 kHz is required).

4.1.2 Comparison between S-TOP and visualization results. Figure 18 shows the at comparison between the results measured by the S-TOP and those obtained from the visualization. In this study, we measured two hundred sub-mm-size droplets to evaluate the measurement accuracy of S-TOP. The average droplet velocities via-measured by S-TOP (figureFig. 18 (a)) showed satisfactory agreement with those from the visualization, satisfactorily. The difference of in averaged velocity between the S-TOP calculation and visualization is-was less than 7.2 %. However, the droplet velocities measured by S-TOP have a large dispersion compared with those by the visualization. The dispersion, with a ranges from ± 30 % to ± 60 % of droplet velocities. Furthermore, this dispersion does not depend on the droplet velocity. Figure 18 (b) shows the a comparison of the droplet chord lengths between the S-TOP and the visualization. The average chord lengths viaby S-TOP are larger than those from the visualization. Furthermore, the dispersiontribution ranges from 30 % to 60 %. In the visualization, we obtained the barycentric velocity of the droplets. On the other hand, the S-TOP measured the interface velocity of the droplets. Therefore, the difference between the S-TOP and the visualization results includes a kind of random differences (not as opposed to bias differences) due to uncertain factors (e.g., the primary surface oscillations of the droplets). It is difficult to remove completely remove this these random differences from the measurement results of S-TOP. Based on our results, the number of samples should be larger than 200. (In addition, in these average results, the bias differences described in 3.1.2 are not removed.)



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コメント [KN17]: Why do you use "distribution" here and "dispersion" for velocity? "Distribution is the more common statistical term.

コメント [KN18]: Do you mean "should not be"? Or are you just informing reader (if so, keep as is)



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4.2 fs-Probe<u>Fs-TOP</u> measurement.

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4.2.1 Comparison between <u>fs-ProbeFs-TOP</u> and visualization results (mm-size droplets). The⁴ droplet velocity calculated from equation (5) and the chord lengths calculated from equation (6) were compared with those obtained from the visualization. The droplet chord lengths from the visualization were calculated based on the projected areas. The comparison is listed in Table 1 and summarised in <u>figureFig.</u> 19. The <u>fs-ProbeFs-TOP</u> results <u>on_for_droplet</u> velocities and chord lengths are less than those from the visualization. When the droplet velocities are smaller than 2.0 m/s, the droplet velocities <u>via_by_fs-ProbeFs-TOP</u> is are approximately 5 % (bias difference) smaller than those <u>via_by_visualization</u>. However, when the droplets velocities are higher than 2.0 m/s, those <u>via_by_visualization</u>. The number of samples was random 10 of 100. The dispersion of the other 10 samples has had the a similar distribution. The dispersion observed in the droplet velocities rangeds from ± 12 % (at 2 m/s) to ± 20 % (at 0.26 m/s). This dispersion decreases with increase in droplet velocity. This property is very different from the that of S-TOP (see 4.1.2).

The chord lengths measured by <u>fs-ProbeFs-TOP</u> include the randomness due to piercinge position (however-within the centre region of <u>the</u>_droplets) and those due to <u>the</u>-surface oscillation. Furthermore, they include randomness propagated from velocities; the chord length is calculated from velocity (equation (6)). The chord lengths obtained from the visualization include randomness due to the surface oscillation. Figure 19 (b) shows <u>the-the</u> relation of chord-length dispersion to droplet velocity for both-between the <u>fs-ProbeFs-TOP</u> and the visualization, <u>against the droplet velocity</u>. The dispersion of <u>the fs-ProbeFs-TOP</u> results is wider than that of the visualization. The dispersion is not influenced by the velocity.

35 400 4.2.2 Com ProbeFs-T <u>OP</u> and visualization results (sub-mm-size and <u>um-</u> parison between f 18125 *droplets*). The con arison of measurement results of for sub-mm-size dropets 20 and visualization is are listed in Table 2 and also OP 15 summaris average results of the fs-P The robeFs-TOP on_for droplet 20 velocifies chord lengths were approx anately 10 % less than those from the and Ś 0₀ (by 25 5 10 15 20 200 $U_{\rm D}$ (by visualization) [m/s] L_D (a) Droplet velocities. - 29 -100 10 20 U_D (by visualization) [m/s]



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(b) Droplet chord lengths.

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visualization (this difference is a kind of bias). The velocity dispersion of <u>fs-ProbeFs-TOP</u> (<u>figureFig.</u> 20) <u>is-was_very-much_smaller</u> than that <u>viaby</u> S-TOP (see <u>figureFig.</u> 18). From <u>figureFig.</u> 20, the velocity dispersion of <u>the fs-ProbeFs-TOP</u> decreases with <u>the</u> increase in the droplet velocity even in sub-mm-size measurements. Those tendencies of the measurement results of the sub-mm-size droplets are the same tendency <u>of for</u> those of the mm-size droplets. However, the dispersion of the measurement results of sub-millimetre droplets is smaller than those that of the millimetre-size droplets. (<u>In addition, iI</u>n these average results, the bias differences described in 3.1.2 are not removed.)

Measurement results of the <u>um-size-micrometre-size</u> droplets are shown in <u>figureFig.</u> 21. The results of droplet velocity <u>via-by fs ProbeFs-TOP</u> are smaller than those <u>of theby</u> visualization. Furthermore, the measurement results of the droplet chord lengths are also smaller than those from the visualization. (In these average results, the bias differences described in 3.1.2 are not removed.) Considering that S-TOP can not measure <u>um-size-micrometre-size</u> droplets, the <u>fs-ProbeFs-TOP</u> has-demonstrated satisfactory performance <u>of in</u> measuring velocities and chord lengths of <u>um-size-micrometre-size</u> droplets.

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5. Conclusion

In this paper, we describe the characteristics and performance of the Fs-TOP, a newly⁴ developed single-tip optical fibre probe micro-processed by femtosecond pulse laser. We also

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4. Conclusion

In this paper, we described the characteristics and performance of <u>the S TOP and fs Probe (:,</u> a newly developed single <u>single_tip</u> optical fibre probe micro-processed by femtosecond pulse laser). We <u>also</u>_compared those the characteristics of the <u>fs-ProbeFs-TOP</u> and <u>S-TOP</u> in detail, in order to present guidelines in order to allow researchers in various fields to selectfor effective_the appropriate probe for a particular applications of those to various targets. Their eCharacteristics, performance and measurement accuracies were evaluated based on the comparisons of the <u>probe</u> measurement results between the <u>S-TOP</u>/fs Probe_ and <u>with</u>

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visualization<u>results</u>. The <u>fs-ProbeFs-TOP</u> has satisfactory performance and accuracy for measurements of <u>um-size</u> micrometer size droplets. Our investigation is summarized as follows.

For the specific purpose of reduc<u>ingtion of</u> the random errors due to piercing position, we proposed a new method <u>using a pre-signal</u> to detect whether the S-TOP/fs-ProbeFs-TOP pierces the centre region of a droplet/bubble-by using the pre-signal. The random errors are less than 5 % of the minor axes of the-droplets with 50 μ m – 2 mm in equivalent diameter.

The forced surface deformation of the droplet when the probe touches the droplet surface is very small for droplets with $50 - 500 \mu m$ in equivalent diameter. Hence, this surface deformation is negligible for the droplets in the above this diameter range.

The deformation of the <u>a</u> droplet pierced by the <u>either</u> probes is very small during measurement. In the case of sub-mm-size droplet measurements, the deformation is <u>smaller</u> <u>less</u> than 3.2 % of droplets' minor axes (this <u>a bias</u> difference is a kind of bias), and in the case of <u>um-size</u> <u>miero-size</u> droplet measurement, it is smaller than 3.1 % of droplets' minor axes (this difference is a kind of a bias difference).

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Figure 21. Comparison of <u>fs-Probe</u> measurement results of <u> μ </u>micrometre-size droplets between fs-Probe and visualization results.

On the basis of these results, first, we described the characteristics and performance of S TOP. In the measurement of sub mm size droplet, <u>s</u>, the difference of <u>in</u> averaged velocity between⁴ ^{- -} ⁻ the S-TOP and visualization is less than 7.2 % (in these average results, the bias differences described in above are not removed). However, the droplet velocities and chord lengths

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measured by S TOP have a large dispersion compared with those by the visualization. dispersion ranges from ± 30 % to ± 60 % of droplet velocities. Furthermore, the average chord lengths viaby S TOP are larger than those from the visualization. TIn addition, those distribution ranges are also from 30 % to 60 %. As the reason of this, the S TOP measured the interface velocity (not barycentric velocity) of the droplets. Therefore, the difference between the S-TOP and visualization results includes a kind of random differences (not bias) due to uncertain factors (e.g., the primary surface oscillations of the droplets). It is difficult to remove completely remove this random difference from the measurement results of S TOP. Based on our results, we suggested that the number of samples of thefor S-TOP measurement have should be larger than 200 to measure the droplets in obtain high_ accuracy results.

we described the performance and properties of the S-TOP/fs-Probe by examining mmsize droplets, and sub mm size droplet. The dispersion of the measurement results of submm-size droplets is was smaller than those that of mm size droplets. In the measurement of sub-mm size droplets, the average results of the fs Probe for on droplet velocities and chord lengths ware ere approximately 10 % less than those from the visualization (this a bias difference is a kind of bias). Moreover, the velocity dispersion of by fs Probe is was very much smaller than that via by S TOP. The velocity dispersion of fs Probe decreases decreased with an increase in the droplet velocity, in both of the mm size droplet and sub mm size droplet measurements.

In addition, we demonstrated the measurement of velocities and chord lengths of micrometresize droplets using the fs-Probe. The results of for droplet velocity via by fs-Probe are were smaller than those byof the visualization. Furthermore, the measurement results of the droplet chord lengths are were also smaller than those from the visualization (in these average results, the bias differences described in above are were not removed). Considering that S-TOP can measure micrometre-size droplets, the fs-Probe has demonstrated satisfactory performance of measuring velocities and chord lengths of micrometre size droplets. As above, each optical probe (S TOP/fs Probe) has different kinds of characteristics. In this paper, we clarifiedy the application range of S-TOP and fs-Probe quantitatively as follows::

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1) The measurement object of the S-TOP is the a sub-mm size droplet moving less than 5 m/s. In the cases of measuring the ement of averaged velocity of sub-mm-size droplets, the desirable sample number of for the S-TOP is larger greater than 200.

2) The measurement object of the fs Probe is the micrometre-size droplet and sub-mm-size droplets moving at over speeds of 5 m/s or more. In the cases of measurement of measuring the averaged velocity of sub-mm-size droplets, the desirable sample number of for the fs-Probe is more greater than 10.

Nomenclature

| g_{rd} | gradient of the S-TOP signal (s ⁻¹) |
|----------|------------------------------------------------------------------------------------------------|
| L_D | chord length pierced by Probe (mm or µm) |
| L_P | length between tip and groove of the $\underline{\text{fs-Probe}Fs-TOP}$ (mm or $\mu\text{m})$ |
| t | time (s or ms) |
| V | output of a photo multiplier (V) |
| U_D | interface velocity (m/s or mm/s) |
| | |

Greek symbol

proportionality coefficient (m) α

Subscripts

| 2 | at groove |
|--------|--------------------|
| f | end of contact |
| Gas | gas phase level |
| Liquid | liquid phase level |
| min | minimum output |
| s | start of contact |

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Figure 1. Structure of S-TOP.

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Figure 2. Close-up photograph of fs- <u>ProbeFs-TOP for sub-mm-size droplets</u>.



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Figure: 3. The sS chematic diagram of measurement processes of the S-TOP and fs-ProbeFs-TOP.

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(a) Probe, (b) Optical stages, (c) Optics,
-(d) Recorder, (e) High-speed video camera,
(f) PC, (g) Halogen light,
(h) Needle, (i) Droplet Figure 5. Experimental

(a) Probe, (b) Optical stages, (c) Optics, (d) Recorder, (c) High-speed video comera (f) PC, (c) Halogen light (h) Naedla (i) Droplet

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(a) Pressurization source, (b) Water tank, (c) Pressure controller, (d) Electromagnetic valve, (e) Piezo nozzle, (f) Digital oscilloscope, (g) Optical system, (h) 3-axis unit, (i) S-TOP, (j) High-speed video camera 1, (k) High-speed video camera 2, (l) Strobe light, (m) Halogen light source.
 Figure 6. Experimental setup for measurement of sub-millimetre-size droplets.



(a) Probe, (b) Optical stages, (c) Optical system, (d) Digital oscilloscope,
(e) High-speed video camera, (f) PC, (g) Strobe light, (h) Piezoelectric ink jet nozzle,
(i) Droplet,
(j) Controller, (k) Monitor, (l) Water tank

Figure 7. Experimental setup for measurement of μmicrometre-size droplets.
 (a) Probe, (b) Optical stages, (c) Optical system, (d) Digital oscilloscope,
 (e) High speed video camera, (f) PC, (g) Strobe light, (h) Piezoelectric ink jet nozzle, (i)

Droplet,

(j) Controller, (k) Monitor, (l) Water tank

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Figure 8. A typical signal in-for droplet measurements viaby S-

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- ♦ Sub-mm-size droplets $(L_D = 250 \pm 60 \ \mu\text{m})$ ■ Sub-mm-size droplets $(L_D = 300 \pm 60 \ \mu\text{m})$ • Sub-mm-size droplets $(L_D = 500 \pm 60 \ \mu\text{m})$ • Medium-size droplets $(L_D = 2500 \pm 30 \ \mu\text{m})$
- \triangle Medium-size droplets ($L_D = 5000 \pm 60 \ \mu m$)

Figure 9. The relationship between g_{rd} and U_D (visualization) rearranged by using α of

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(b) <u>Snapshots:</u> The fs-Probe touching a sub-mm<u>-size</u> droplet moving at a high velocity (10m/s);

Figure 11. Snapshots of touching process under different conditions.

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Figure 12. Flow chart of the signal processing employed.

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Figure 13. Flow chart of the signal processing of the <u>fs-ProbeFs-TOP</u>.



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Figure 14. An examplsample of the histograms of output voltage of fs-Probe signals.

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Figure 15. Schematic diagram of signal processing for fs-Probe.



Figure 17. Typical samples of S-TOP signals.



| (a) Averag | ge droplet v | velocities | (b) |) Average dropl | et chord le | ngths |
|---------------|--------------|-------------|------------|-----------------|-------------|-------------|
| Visualization | fs-Probe | Differences | Velocities | Visualization | fs-Probe | Differences |
| [m/s] | [m/s] | [%] | [m/s] | [mm] | [mm] | [%] |
| 0.279 | 0.271 | -2.8 | 0.28 | 2.89 | 2.48 | -16.3 |
| 0.681 | 0.653 | -4.3 | 0.68 | 2.65 | 2.77 | 4.2 |
| 1.069 | 1.040 | -2.8 | 1.07 | 2.77 | 2.53 | -9.5 |
| 1.434 | 1.350 | -6.2 | 1.43 | 2.20 | 2.48 | 11.4 |
| 1.776 | 1.691 | -5.0 | 1.78 | 2.79 | 2.68 | -4.1 |
| 2.210 | 1.989 | -11.1 | 2.21 | 2.21 | 2.04 | -8.6 |
| | | | | | | |

 Table 1. Differences between fs-ProbeFs-TOP and visualization results (mm-size droplets).

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Figure 19. Comparison between <u>fs-ProbeFs-TOP</u> and visualization results (mm-size droplets).

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Figure 20. Comparison of <u>fs-ProbeFs-TOP</u> measurement results ______of sub-millimetre-size droplets between

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- - **書式変更:** フォント:太字

| Table 2. Differences of measurement resu | ılts |
|------------------------------------------|------|
| of sub-millimetre-size droplets | |
| between <u>fs-ProbeFs-TOP</u> | and |
| visualization | |

I

| Visualization | Fs-TOP | Differences |
|---------------|--------|-------------|
| [m/s] | [m/s] | [%] |
| 4.77 | 4.32 | -9.5 |
| 5.35 | 4.95 | -7.5 |
| 6.49 | 6.05 | -6.8 |
| 7.59 | 7.33 | -3.5 |
| 8.55 | 7.76 | -9.2 |
| 9.46 | 8.49 | -10.3 |
| | | |



Figure 21. Comparison of <u>fs-Probe</u> measurement results of μ micrometre-size droplets between fs-Probe and visualization results.

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