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2 **Practical Method to Estimate the Standard Deviation in Absorption Coefficients**  
3 **Measured with THz Time-Domain Spectroscopy**  
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44 **Abstract:**

45 A model of standard deviation in the intensity spectrum of electric field observed with the  
46 terahertz time-domain spectroscopy (THz-TDS) is proposed to estimate the random error in the  
47 transmittance and absorption coefficients from a single or a few measurements of a sample. The  
48 proposed standard deviation which is derived on the basis of the statistical standard deviation  
49 and noise floor of intensity spectrum of reference fits well to the standard deviation of  
50 transmittance as well as absorption coefficient computed statistically. This study contributes the  
51 simple and computationally efficient method to demonstrate the accuracy in optical constants  
52 like imaginary part of refractive index and absorption coefficients measured using the  
53 THz-TDS.  
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3 **Keywords:**

4 Terahertz wave, THz time-domain spectroscopy, optical constant, random error

5 **Classification codes:**

6 87.64.k-; 78.20.ci; 29.85.Fj  
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10 **1. Introduction**

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12 Terahertz time-domain spectroscopy (THz-TDS) has been widely used to study the  
13 spectroscopic characteristics of the variety of the materials [1-3] like dielectrics [4],  
14 semiconductors [4-5], bio-molecules [6], liquids [7], pharmaceutical products [8] and so on in  
15 the spectral region spanning from 0.1 to 3 THz. Most spectroscopic measurements involve the  
16 recording of a time-domain pulse of THz electric field transmitted through a sample under  
17 investigation placed on the path of the terahertz radiation and a reference signal recorded in the  
18 absence of the sample. The time-domain waveforms are converted to the frequency-domain by  
19 the complex Fourier transform to obtain the intensity and phase spectra. These spectra are  
20 processed further to calculate the transmittance and phase differences which are used to derive  
21 the frequency dependent dielectric properties like complex refractive index, complex dielectric  
22 constant and absorption coefficient.  
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28 The measured spectra of sample and reference electric fields using THz-TDS and the  
29 dielectric properties (also called as optical constants) obtained using these electric fields are  
30 prone to have systematic and random errors and the precision is limited by them [e.g., see ref. 9].  
31 The systematic error is due to error in measure of sample-thickness measurements (including  
32 parallelism and roughness of the surfaces), sample misalignment, error in optical delay distance  
33 etc. and these errors could be eliminated or reduced to some extent by making effort in sample  
34 preparation, spectrometer calibration and so on. However, the random errors which are caused  
35 mainly by laser power fluctuation, electronic noise in devices, optical and mechanical instability  
36 can not be removed completely and it becomes necessary to quantify them with statistical  
37 analysis by taking number of observations.  
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43 Previously, a method to identify the dynamic range from one reference spectrum and the  
44 detectable limit of absorption coefficient from the sample spectrum has been reported [10], but  
45 this does not provide the information on the random error in measured data. The methodology  
46 to determine the standard deviation in intensity spectrum has been reported by taking large  
47 number of measurements [11]. As one scan of measurement in THz-TDS requires several to ten  
48 minutes, more than several hours are necessary to take enough number of sample and reference  
49 data for evaluating the statistical standard deviations in the measured optical parameters with an  
50 ordinary frequency resolution, which is usually difficult and not practical to execute always for  
51 many samples. One or a few pair of reference-and-sample data are usually expected to obtain  
52 the optical parameters of each sample by the THz-TDS, in which case the estimation of errors  
53 can not be done by statistical methods. Therefore, in this study we provide the method to  
54 estimate the error in the transmittance and absorption coefficient even if a sample is measured  
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2 only one time with THz-TDS by using the statistical standard deviations in the intensity spectra  
3 derived from many number of reference data.  
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## 7 **2. Measurements**

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9 We took a number of reference and sample time-domain waveforms with a THz-TDS system to  
10 examine the error characteristics in the measured data. The THz-TDS system used for the  
11 measurement is the Rayfact Spectera [12] (Tochigi Nikon Corporation) consisting of a compact  
12 femto-second fiber laser (Femtolite, IMRA Inc.) with a pulse width of less than 100 fs and 20  
13 mW average power and LT-GaAs photoconductive antennas as THz emitter and detector. Three  
14 ZnTe crystals with different thickness (0.767 mm, 1.496 mm and 2.976 mm) supplied  
15 commercially by Nippon Mining and Metals Co. Ltd. [13] are used as samples and they have  
16 very low absorption coefficient in the frequency range of 0.2 to 3 THz [14]. The time-domain  
17 data of 1024 points is taken in one scan of time delay line with the frequency resolution of 0.024  
18 THz ( $0.814 \text{ cm}^{-1}$ ), which needs about 10 minutes for each scan. The data is observed in the  
19 sequence like  $R_0, S_0, S_1, R_1, R_2, S_2, \dots, R_k, S_k, \dots, S_{m-1}, S_m, R_m$ , where R and S are the reference  
20 and sample data respectively, and k and m of subscripts are integers. The  $R_k$  and  $S_k$  with the  
21 same subscript means a pair of reference and sample data which are close to each other in time  
22 at which they are measured. Twelve, sixteen and sixteen data sets of reference and sample  
23 waveforms were recorded for the 0.767 mm, 1.496 mm and 2.976 mm thick ZnTe crystal  
24 respectively.  
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## 34 **3. Derivation and modeling of standard deviation**

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36 The time-domain pulses of electric field suffered from the random error are characterized  
37 by the temporal shift of pulse position and pulse shape, which are approximately represented by  
38 a position in time and amplitude of the largest pulse in the waveform respectively. The variation  
39 in position and amplitude of the peak depend on time of an order of hour, which showed good  
40 correlation between reference and sample data. It is possible to correct the variation in position  
41 and amplitude of the largest peak pulse by performing a data processing prior to taking Fourier  
42 transform. We therefore adjusted the waveforms so that respective peak amplitude become  
43 equal to the averaged peak height. After conversion of the waveform data from time-domain to  
44 frequency-domain by the Fourier transform, this pre-process have brought a good effect to  
45 improve the standard deviation in the intensity spectra. As a result, the standard deviation in the  
46 transmittance derived through the error-propagation from reference and sample spectra has  
47 become almost equal to the statistical standard deviation which is calculated from the  
48 transmittances obtained using each pair of reference and sample spectra. In other words, this  
49 means the data taken more closely in time has smaller variances.  
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57 The intensity spectra of reference and sample are derived by the procedure explained above  
58 for the ZnTe crystals with three different thicknesses. Figure 1 displays the average of 12 data  
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3 of 0.767 mm ZnTe sample and reference spectra along with their respective standard deviations  
4 calculated by statistical mathematics. Beyond the detectable upper frequency limit, the intensity  
5 spectrum approaches a flat noise level, which is called as the noise floor [10,15]. The intensity  
6 spectra of reference and sample have the noise floor above 7 THz and 4.5 THz respectively. The  
7 remarkable feature in Fig.1 is that the standard deviations of reference and sample are much  
8 higher than the level of noise floor in the larger intensity region and they are correlated with the  
9 respective intensity; the intensity of the sample is smaller than that of the reference due to  
10 attenuation caused by the ZnTe crystal and hence the standard deviation of former is smaller  
11 than latter's. Spectra of intensity and standard deviation of the reference as well as sample show  
12 that the signal-to-noise ratio (SNR) is rapidly improved with an increase in the intensity from  
13 the noise floor to a higher level, but the SNR nearly becomes to be unchanged in the high  
14 intensity region.

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16 We therefore assume the simple relation between the standard deviation and the intensity as  
17 expressed in Eq.(1), implying that the standard deviation is proportional to the intensity and  
18 approaches to the noise floor at the lowest intensity signal region.

$$19 \quad \sigma_I(\omega) = C(I(\omega) - h) + h \quad (1)$$

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21 where  $\omega$  is angular frequency,  $\sigma_I(\omega)$  is the standard deviation of the intensity,  $I(\omega)$  is the mean  
22 intensity,  $h$  is the noise floor, and  $C$  is assumed as a proportionality constant. We calculated the  
23 values of  $C$  from the standard deviation and intensity spectra of reference and sample using Eq.  
24 (1) to verify its validity. Figure 2 shows the values of  $C$  decrease from the higher frequency to  
25 lower frequency, meaning that SNR is improved, and increase a little below 1 THz, implying  
26 the SNR becomes worse though the intensity still increases there. These facts suggest that the  
27 SNR is almost unchanged around the high intensity region, and hence the standard deviation  
28 becomes explicitly proportional to the intensity and  $C$  can be taken as a constant independent  
29 from frequency. Eq. (1) provides the simplest computational model using the constant  $C$  to  
30 derive the standard deviation from the intensity spectrum. The value of  $C$  does not depend on  
31 samples, since it is common in the reference and sample as shown in Fig. 2. Therefore, it can be  
32 determined by the intensity and standard deviation spectrum of only the reference in the high  
33 intensity signal region. The origin of intensity-correlated random error in THz signal is  
34 presently unknown, but it is possibly related to the emission or detection process of THz wave  
35 because intensity fluctuation of femto-second fiber laser as well as its variation during the time  
36 delay scanning are much smaller than the observed standard deviation in the THz signal.

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38 If we know the  $C$  and the noise floor for a sequence of reference intensity spectrum  
39 measured with a THz-TDS, we can estimate the standard deviation of the sample intensity  
40 spectrum even if it is taken only one time. We can afford to measure different samples in the  
41 data-taking sequence of  $R_0, S_0, S_1, R_1, R_2, S_2, \dots, R_k, S_k, \dots, S_{m-1}, S_m, R_m$  though the reference  
42 data should be continuously taken under the same condition.

#### 4. Estimation of standard deviations in transmittance and absorption coefficients.

Transmittance was calculated as  $T(\omega) = I_S(\omega)/I_R(\omega)$  from a pair of sample and reference intensity spectra,  $I_S(\omega)$  and  $I_R(\omega)$ , and the average and standard deviation of the transmittance was calculated by statistical mathematics from the 12 data set of the 0.767 mm thick ZnTe sample and reference as shown in Fig. 3. Such a standard deviation is called hereafter as the statistical  $\sigma_T$ . It can be seen that the statistical  $\sigma_T$  in transmittance becomes almost equal to the transmittance above around 3.2 THz which is the detectable upper frequency limit of the transmittance.

We calculated the standard deviation in the intensity spectrum of 0.767 mm thick ZnTe sample and the corresponding reference using Eq. (1) by taking the constant  $C$  as 0.0125. The standard deviation thus calculated is referred hereafter as the estimated  $\sigma$ . The estimated  $\sigma$ 's of the reference and sample are denoted as  $\sigma_R$  and  $\sigma_S$ , by which  $\sigma_T$  is also calculated using the error-propagation law [16] as

$$\sigma_T = T(\omega) \left( \frac{\sigma_R^2}{I_R^2(\omega)} + \frac{\sigma_S^2}{I_S^2(\omega)} \right)^{1/2}. \quad (2)$$

The estimated  $\sigma_T$  is displayed together with statistical  $\sigma_T$  in Fig. 3. This figure shows the estimated  $\sigma_T$  is well fitted to the statistical  $\sigma_T$  within the factor of 2 between 0.2 and 3 THz. The evaluation of such standard deviation made by the simple model is probably sufficient for the measurements of most samples. We believe the proposed model is important and beneficial to the THz-TDS which has difficulty in gathering enough number of reference-and-sample spectra for calculating the statistical standard deviation.

For comparison, in Fig. 3, we show also a standard deviation in transmittance calculated through the error propagation on the assumption that the noise floors of references and sample are equal to the respective standard deviation in all frequencies and such a standard deviation is called as the  $\sigma_T$  from the noise floor. The  $\sigma_T$  from noise floor is also coincides with the transmittance above around 3.2 THz but it is far from the statistical  $\sigma_T$  and the estimated  $\sigma_T$  in the high intensity signal region, indicating that the true standard deviation cannot be derived from the noise floor.

The complex refractive index  $n_c(\omega) = n(\omega) + ik(\omega)$ , where  $n(\omega)$  and  $k(\omega)$  are real and imaginary parts respectively, is calculated from the transmittance and the phase difference between sample and reference signal through iteration calculation. Absorption coefficient is derived from the imaginary part of refractive index by the equation below, where  $c$  is the speed of light.

$$\alpha(\omega) = \frac{2\omega k(\omega)}{c} \quad (3)$$

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2 The statistical standard deviation in absorption coefficient  $\sigma_\alpha$  is calculated statistically using a  
3 number of the derived absorption coefficients.  
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5 The estimated  $\sigma_k$  of the imaginary part of refractive index can be computed from the  
6 estimated  $\sigma_T$  using the error-propagation law assuming  $\sigma_k$  is mainly originated from the random  
7 error in  $T(\omega)$  by Eq. (4).  
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$$\sigma_k = \frac{c}{2d\omega} \cdot \frac{\sigma_T}{T(\omega)} \quad (4)$$

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12 where  $d$  is a thickness of the sample. Using general law of the error propagation again, the  
13 estimated  $\sigma_\alpha$  in absorption coefficient can be calculated as  
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$$\sigma_\alpha = \left( \frac{2\omega}{c} \right) \sigma_k \quad (5)$$

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18 Figures 4(a), 4(b) and 4(c) display the absorption coefficients  $\alpha$  in  $\text{cm}^{-1}$ , the statistical  $\sigma_\alpha$  and  
19 the estimated  $\sigma_\alpha$  of the 0.767 mm, 1.496 mm and 2.976 mm-thick ZnTe samples respectively.  
20 The value of constant  $C$  obtained from the reference data taken during the measurement of these  
21 samples were 0.0125, 0.0139 and 0.0096 respectively, which are rather close but a little  
22 different from each other. This is because the same THz-TDS instrument is used in the  
23 measurements, but the condition of the spectrometer and the environment of the measurement  
24 are somewhat changed due to the different measurement date. The estimated  $\sigma_\alpha$ 's calculated by  
25 the method proposed here are well fitted to the statistical  $\sigma_\alpha$ 's for all samples with different  
26 thickness, though the detectable frequency limit in the absorption coefficients are depend on the  
27 sample thickness as shown by the vertical dashed line in Fig 4.  
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## 35 5. Conclusions

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37 This study proposes a method to estimate the standard deviation in the intensity spectrum  
38 measured with the THz-TDS, implying a model of the standard deviation which is proportional  
39 to the intensity at high intensity signal regions and become equal to the noise floor at higher  
40 frequencies where the signal is completely buried in the noise. The standard deviations in  
41 transmittance as well as in the absorption coefficient can be derived from the standard  
42 deviations estimated with the model using the intensity spectra of the reference and sample by  
43 the error propagation law. The estimated standard deviations fitted well to the standard  
44 deviations calculated by the statistical mathematics. This study makes it possible to estimate the  
45 accuracies in the transmittance and the optical constants like absorption coefficients obtained  
46 from one set of reference and sample data measured with the THz-TDS if we know the constant  
47  $C$  in the model which can be derived from a number of the reference data.  
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3 **Figure captions**  
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5 Figure 1.  
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7 Frequency-domain reference and sample signals and their standard deviations.  
8 Curves **a** and **b** show the averaged intensity spectra of the reference and sample  
9 and curves **c** and **d** are their respective standard deviations.  
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13 Figure 2.  
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15 Values of  $C$  calculated at various frequencies from the intensities and standard  
16 deviations of reference and the 0.767 mm-thick ZnTe sample using Eq. (1).  
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20 Figure 3.  
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22 Transmittance of 0.767 mm-thick ZnTe sample and its standard deviations.  
23 Curve **a** shows the transmittance, curves **b** and **c** and are the standard deviations  
24 of transmittance computed by the proposed method, statistical mathematics, and  
25 curve **d** displays the standard deviation from noise floor for comparison. The  
26 vertical dashed line shows the detectable frequency limit in the transmittance.  
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31 Figure 4.  
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33 Absorption coefficients of (a) 0.767 mm (b) 1.496 mm (c) 2.976 mm-thick  
34 ZnTe samples and their standard deviations computed from the proposed model  
35 and statistical mathematics. The vertical dashed line shows the detectable  
36 frequency limit in the absorption coefficients. The frequency limit decreases  
37 with the sample thickness.  
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Figure 1.

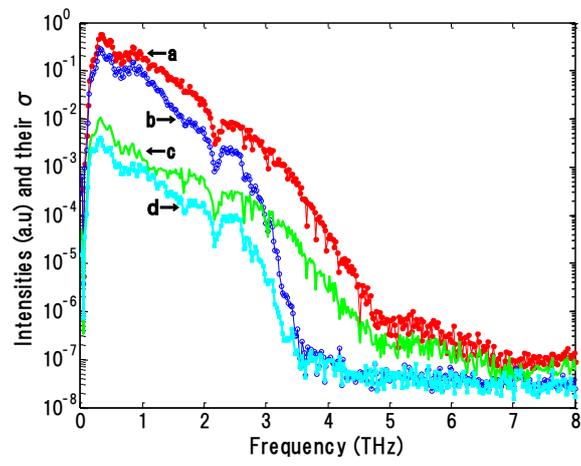


Figure 2

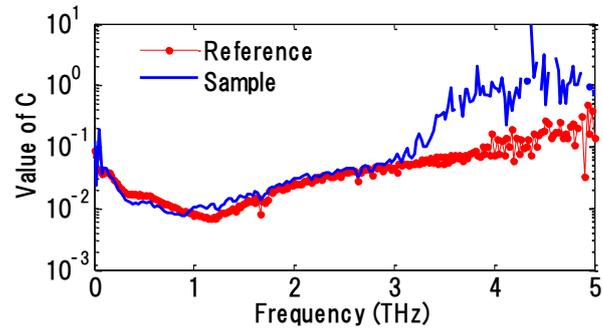


Figure 3

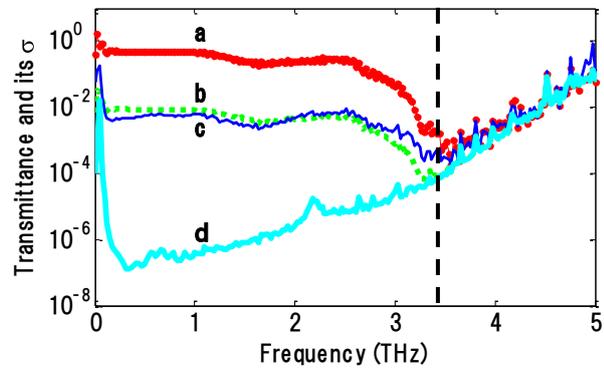


Figure 4.

